



**Cellulose Nanofibrils reinforced Castor oil based
Polyurethane Shape Memory Nanocomposites for
Medical Applications**

**File no. 42-402/2013 (SR)/ March 31, 2013
Final Completion Report**

Submitted to



ज्ञान-विज्ञान विमुक्तये

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Final Completion Report

1. Project report Final
2. UGC Reference No. F. 42-402/2013 (SR)/ March 31, 2013
3. Period of report: from April 2013 to March 31, 2017
4. Title of research project **Cellulose Nanofibrils reinforced Castor oil based Polyurethane Shape Memory Nanocomposites for Medical Applications**
5. (a) Name of the Principal Investigator **Prof. Anupama Sharma**
(b) Deptt. **SSB University Institute of Chemical Engineering and Technology, Panjab University, Chandigarh India-160014**
- (c) College where work has progressed **SSBUICET, Panjab University**
6. Effective date of starting of the project **April 2013**
7. Grant approved and expenditure incurred during the period of the report:
 - a. Total amount approved **Rs. 14,27,217/-**
 - b. Total expenditure **Rs. 13,57,663/-**
 - c. Report of the work done: (Please attach a separate sheet) **Attached as Annexure 1**

i. Brief objective of the project

- 1. Develop fundamental understanding of routes of synthesis of segmental polyurethanes from castor oil**
- 2. Synthesizing biodegradable segmental polyurethanes with shape memory properties**

Synthesize a series of biodegradable segmental polyurethane elastomers based on castor oil with tunable glass transition temperature and degradation rates and potential applications in biomedical implants.

Segmental Polyurethanes will also be synthesized using some largely available polyol (Poly(ϵ -caprolactone) diol) in order to compare the properties of Castor oil based and commercial polyol based polyurethanes.

These new polyurethanes will be characterized by FTIR, NMR, DSC, XRD, uniaxial tensile tests and DMA to evaluate chemical, physical, mechanical and structural properties. The required glass transition temperature (T_g) for these polymers is between 35-53°C which is in the vicinity of body temperature and recovery ratio more than 95%.

3. Study interfacial interactions between shape memory polyurethanes and nanocellulose fibers to achieve good dispersion and for reinforcement of polyurethanes. Study mechanism of polymer formation in the presence of nanocellulose fibers.

4. Reinforcing biodegradable polyurethanes with cellulose nanofibrils to improve the shape memory behavior and thermal properties

Mixing of cellulose nanofibrils in polyurethane matrix will be done during prepolymer stage by high shear mixing in an internal mixer so that the fillers are well dispersed in the matrix. The uniform distribution of the particles will be established using XRD (SAXS and WAXS) and microscopy (SEM and TEM). The improvement in shape memory will also be evaluated in terms of creep and thermal response (mechanical tests). Rheological behavior (plate-plate and cone-plate rheometers) of the materials will be evaluated to better understand the structure and processability of the nanocomposites.

5. Establishing the biodegradability and biocompatibility of these biodegradable shape memory polyurethane composites by in vitro studies

To undertake in-vitro (cell culture) studies for the new biomaterials; thus generating a strong biocompatibility knowledge base

6. Comparison of developed biodegradable shape memory polyurethane composite with existing material used for biomedical implants

ii. Work done so far and results achieved and publications, if any, resulting from the work

(Give details of the papers and names of the journals in which it has been published or accepted for publication)

Details of work done is given in Annexure 1

1. Gaurav Verma, Anupama Kaushik, Anup Ghosh, Nano-interfaces between clay platelets and polyurethane hard segments in spray coated automotive nanocomposites, Progress in Organic Coating, Vol 99, 2016; 282-294 (Impact Factor 6.2)
2. Mandeep Singh, Anupama Kaushik, Dheeraj Ahuja, Surface Functionalization of Nanofibrillated Cellulose Extracted From Wheat Straw: Effect of Process Parameters, Carbohydrate Polymers 150: 48-56, 2016 (Impact Factor 11.2)

3. Anupama Kaushik, R Kaur, Thermoplastic starch nanocomposites reinforced with cellulose nanocrystals: effect of plasticizer on properties, *Composite Interfaces* 23 (7), 701-717, 2016 (Impact Factor 2.6)
4. Sheetal Monga, A Kaushik, B Gupta, Optimization of Process Parameters for Controlled Ring Opening Polymerization of Lactide to Produce Poly (L-Lactide) Diols as Precursor for Polyurethanes, *Polymer-Plastics Technology and Engineering*, 55(17), 2016 (Impact Factor 2.7)
5. Sheetal Monga, A Kaushik, B Gupta, Synthesis of L-Lactide Based Segmented Polyurethanes, *Polymer-Plastics Technology and Engineering*, 55 (9), 943-948, 2016 (Impact Factor 2.7)
6. Sapana Kumari, Ghanshyam S. Chauhan, Sheetal Monga, Anupama Kaushik and Jou-Hyeon Ahn, New lignin-based polyurethane foam for wastewater treatment, *RSC Advances*, 6, 77768-76, 2016 (Impact Factor 3.9)
7. Anupama Kaushik, Jatinder Kumra, Morphology, thermal and barrier properties of green nanocomposites based on TPS and cellulose nanocrystals, *Journal of Elastomers and Plastics*, (3): 284-299, 2014 (Impact Factor 1.2)
8. Anupama Kaushik, Alka Garg, Castor Oil Based Polyurethane Nanocomposites with Cellulose Nanocrystallites Fillers, *Advanced Materials Research* 856, 309-313, 2014

iii. Has the progress been according to original plan of work and towards achieving the objective. if not, state reasons

Yes, it was according to the original plan.

iv. Please enclose a summary of the findings of the study. One bound copy of the final report of work done may also be sent to the concerned Regional Office of the UGC.

Attaches as Annexure 1

v. Any other information

Nil

SIGNATURE OF THE PRINCIPAL INVESTIGATOR

PRINCIPAL (Seal)

Annexure 1

Summary of the findings

INTRODUCTION

Polyurethanes are the class of polymers that contain urethane groups in their backbone structures (Figure 1) [1]. These are generally obtained by condensation reaction of di-isocyanates and polyol compounds and consist of a two-phase structure: a hard segment and soft segment.

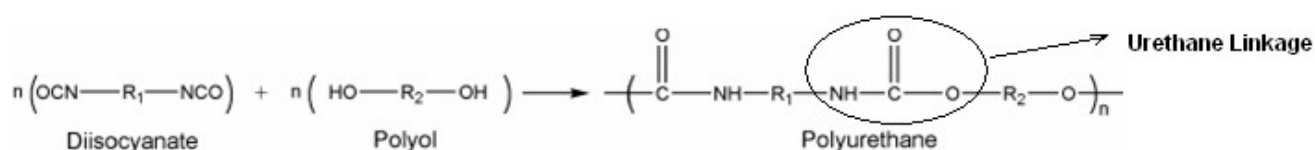


Illustration 1. Polyurethane synthesis process

Polyurethane structure is unique having segmented structure with semicrystalline and rigid 'hard segment' enriched domains that are dispersed in a matrix of crystallizable soft segments (figure 1) [2-4]. *Hard segment* clusters are generally of dimensions $<1 \mu\text{m}$ formed by the phase separation process and these clusters have higher glass transition temperature or melting temperature values than the ones of soft segment and act as multifunctional physical net-points. The amorphous matrix, with its low glass transition temperature, is called *soft segment*. The hard segments mainly consist of the diisocyanate; either aromatic or aliphatic and the chain extender while the soft segments are sequence of macroglycol moieties which are used to maintain the temporary shape [5]. The thermodynamically incompatible hard and soft segments are combined end-to-end through covalent urethane bonds making polyurethanes as multiblock copolymers. Soft segments are generally comprised of polyester, polycarbonate, or polyether macroglycols. Chain extenders may be low molecular weight diols or diamines used to further couple these pre-polymers [6, 7]. The differences in polarity between the hard and soft segments render these regions incompatible and the result is that they do not mix on a molecular level, producing a microphase separated structure.

Segmented polyurethanes are stimuli-responsive materials i.e. their temporary deformation can be eliminated or their permanent shape can be recovered at a critical stimulus value, also known

as shape memory materials having capability of changing their shape upon application of an external stimulus. This stimulus can be heat, stress, magnetic fields, electric fields, pH values, UV light, and even water [8, 9]. The segmented polymer is conventionally processed for its *permanent shape* followed by deformation to the intended *temporary shape*. Finally, the permanent shape is restored through the recovery process. If the change in shape is caused by a change in temperature is called a thermally induced shape memory effect or thermoresponsive shape memory behaviour. Large numbers of chemical and structural factors play important roles in microphase separation and thus response to the stimulus. These factors include Chemical structure, number average molecular weight and molecular weight distribution of soft segments, chemical structure and symmetry of the diisocyanate compound, chemical structure of the chain extender, average chain length and length distribution of hard segments, hard/soft segment ratio in the copolymer [10, 11], crystallizability of hard and soft segments [12], extent of competitive hydrogen bonding between hard-hard and hard-soft segments, inherent solubility between hard and soft segments [13, 14], method/polymerization procedure used during the synthesis and the nature of the interfacial region between the soft segment matrix and hard segment domains [15]. By adjusting the molecular weight of the macrodiol moiety and the molar ratio of the soft-to-hard segment, the shape recovery temperature of polyurethane can be successfully adjusted to 37-40 °C.

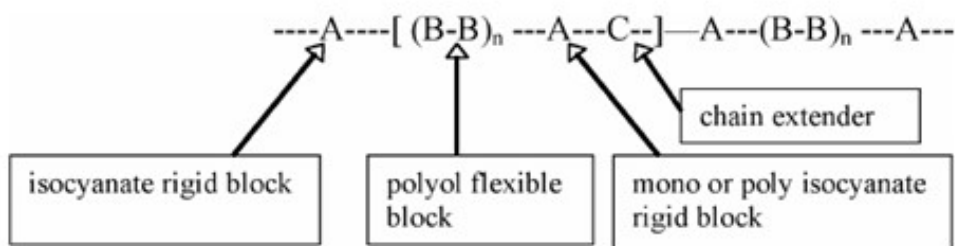


Figure 1: Polyurethane structure showing hard segment dispersed in soft crystallizable phase [16]

Segmented polyurethanes are extensively used polymers in biomedical applications because of their durability, elasticity, fatigue resistance, compliance, bio-stability, biodegradability and tailorable backbone structure from a wide range of available precursors. A thermo-responsive segmented polyurethane get deformed at a temperature above transition temperature (which can be glass transition or melting temperature) and suddenly cooled to a temperature below *transition temperature*, the deformed shape becomes frozen. When it is heated above *transition temperature*, the polymer recovers its original shape [17]. Because of the ability of thermo-responsive segmental polyurethanes to recover shape at critical temperature large bulky devices could thus potentially be introduced into the body in a compressed temporary shape by means of minimally invasive surgery and then expand to their permanent shape to fit as required [18]. This property is very useful in cardiovascular stents and sutures. Conventionally used alloys, like Nitinol, for cardiovascular stents exhibit outstanding features, such as small size and high strength, but show disadvantages like high manufacturing cost, limited recoverable deformation and complicated surgery process [19]. Moreover, metal stents being rigid compared to the surrounding vessel, cause abrupt change of compliance in the junction of the host artery and the stent, lead to an abnormal stress concentration which will initiate an adaptive response in the vascular tissue [20]. Therefore, shape memory polymers have come to the focal point over the last decade as proposed materials for stents [21, 22]. Potential Biodegradability is an additional functionality of shape memory polymers that can prevent a second surgery for device explanation. With good biodegradability, they would neither stay in the human body for a very long time nor require a second surgery to be removed from the human body. With shape-memory property and a recovery near body temperature, the handling of the corresponding medical devices would be easy.

Shape Memory Polyurethanes

Shape-memory materials, including shape-memory alloys, ceramics, hydrogels, and shape memory polymers, have found wide applications in various fields, such as sensors, transducers, actuators and medical implants. In order to qualify as a shape memory material it should possess shape memory effects. Shape memory effects are those in which a material can be deformed and

fixed into temporary shape and can return to original permanent shape under cyclic conditions of loading/unloading and thermal swings. Shape memory effect caused by thermal stimuli are more common as in this the recovery takes place with respect to a certain critical temperature. The first shape memory effect induced smart material was first discovered by Chang and Read in 1932 (Chang and Read 1951). Even though shape memory materials based on alloys possess excellent mechanical properties and have found a ample of technical applications, they have been replaced by ceramics and polymers because of the high manufacturing cost, narrow recoverable deformation and appreciable toxicity.

A great deal of attention is being focused towards shape memory polymers for the development of smart materials because of their varying mechanical properties and higher degree of deformation offered along with low cost, light weight and easy processibility. Further, an added advantage offered by polymers is that they may be resistant to chemical attack, non toxic, biocompatible and can be made biodegradable. Different kinds of shape memory polymers have been reported and developed after the development of “Polynorbornene” the first shape memory polymer developed by CDF Chimie company (France) in 1984.

Shape memory polymers are those that can adopt a new temporary shape and revert back to original shape under the influence of an external stimulus. In these cases, the shape memory performance not only depends on the molecular structure, but also on the mode of deformation and the programming of the stimulus application process. Obtaining a new shape is dependent on both the nature of stimulus and the mode of deformation. On the other hand, regaining the original shape is always dictated by how the stimulus is applied. The stimulus here refers to heat, light, chemical reaction, electricity, and magnetism. This may be applied independently, e.g. only heat or light, or in complex combinations (Beloshenko, Varyukhin, and Voznyak 2005). The process is shown in figure 2.

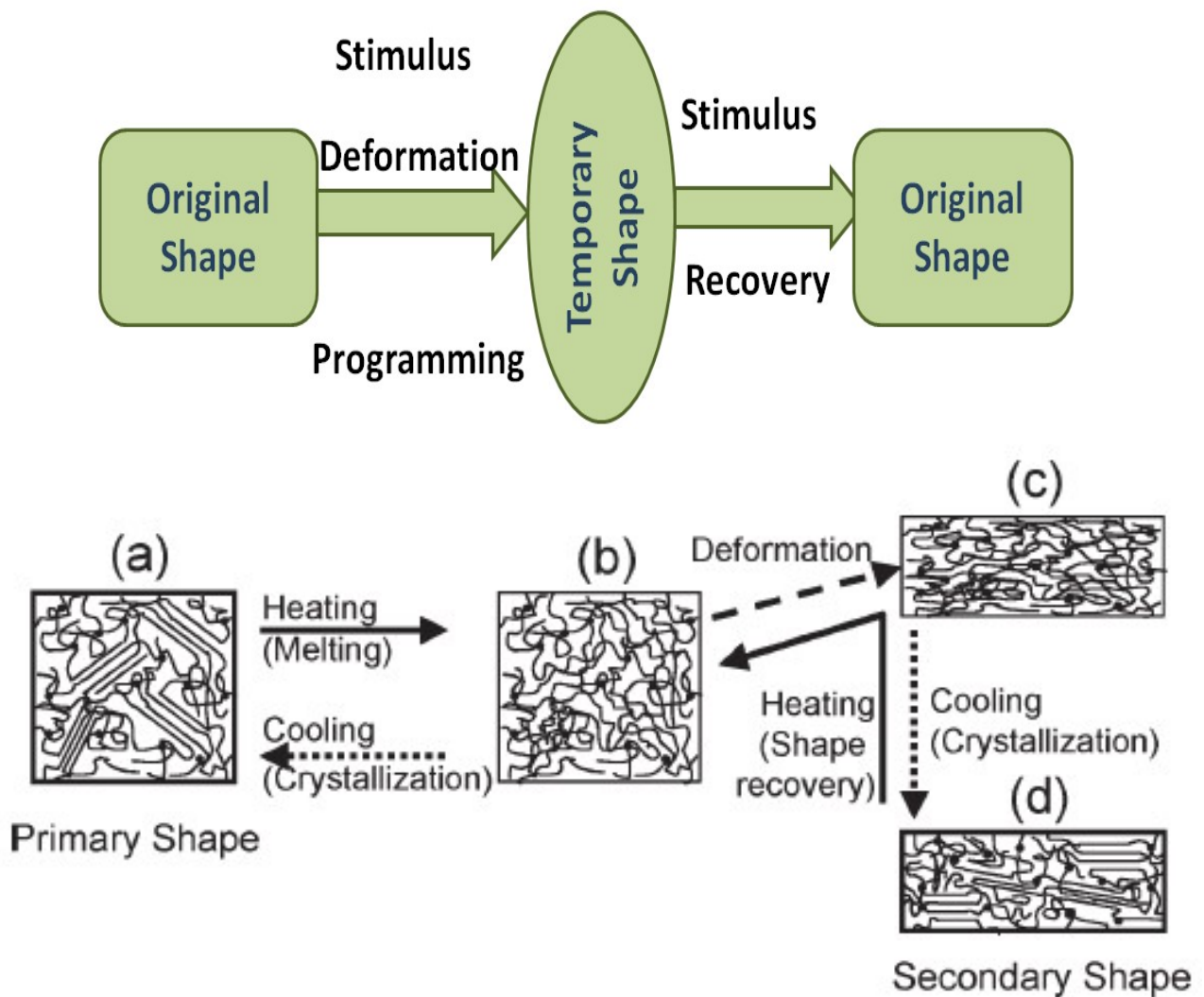


Figure 2: Process of Shape memory polymer

The material having shape memory effects should have at least two independent or synergistically working phases, among which one phase should be reversible while the other shall be in the active range of the stimulus. Therefore, shape memory effects are accomplished during a transition stage i.e. where the reversible phase undergoes changes from temporary to permanent shape and a permanent shape can be achieved by polymer chains on deformation during this transition state. However, it should be noted that on attainment of temporary shape stimulus should be taken away rapidly for achieving the desired form as if the stimulus takes longer time to return to the reference state, polymer chains can relax leading to the poorer shape memory performance. For example, low thermal conductivity of polymers in case of thermal gradients

leads to the slower cooling and heating where the elastically stored energy plays an important role in shape memory performances as the polymer chains store an important part of energy during deformation which is used to recover the original shape upon the application of the stimulus. The heat dissipation is another important factor. Further, an important factor that accounts for shape loss is heat dissipation during deformation and recovery in a single shape memory cycle. However, these types of loss depends on the rheological properties of the materials. Stretching/deformation temperature and extent of deformation/strain level along with rheological properties of polymer are the most critical conditions used to determine the recovery force and extent of shape useful in deciding suitable applications of the shape memory polymers. For example magnitude of recovery stress developed by polymers needs to be evaluated carefully while replacing shape memory alloys with shape memory polyurethanes.

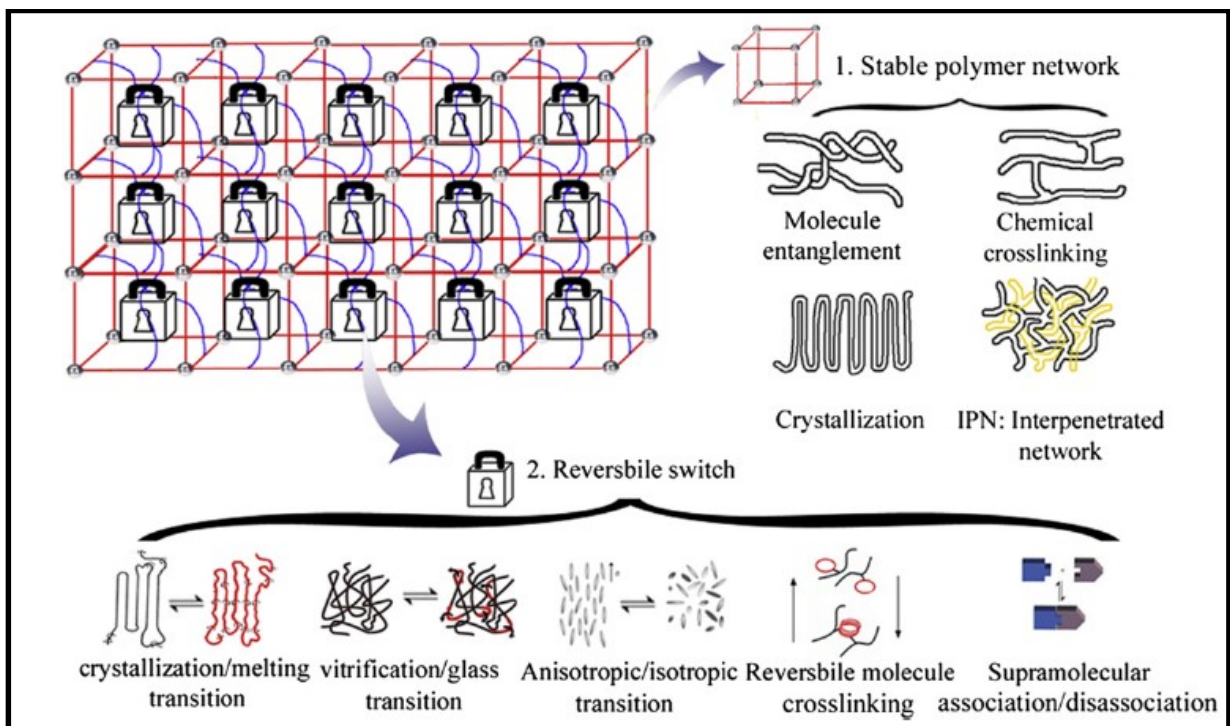


Figure 3. Molecular Structures of Polymers which gives shape memory effect

Shape memory effects are possessed by a variety of polymers such as theroplastics based on polyethylene and polystyrene copolymers and thermosets based on polyurethanes and polyepoxides. Polyurethanes with shape memory effects have become the most popular among these polymers because of their unique properties such as high shape recoverability with a

maximum recoverable strain of >400%, wide range of shape recovery temperature from -30 to 70 °C, good processing ability and excellent biocompatibility. Some other characteristics of the shape memory polyurethanes (SMPU's) that make them prominent material as compared to other shape memory polymers are biodegradability, vast possibilities for synthesis and production from readily available commercial raw materials at affordable cost. Figure 3 elaborates the molecular structure of polymers which contributes to shape memory polymers

Shape memory polyurethanes (SMPU's) are one of the most popular groups of biomaterials applied for biomedical applications which may be attributed to their segmented block copolymeric character that endows them for a wide range of versatility in terms of tailoring their physical properties, blood and tissue compatibility. They are usually thermo-responsive, i.e., their temporary deformation can be eliminated and their permanent shape can be restored at a critical temperature (referred as transition temperature or switching temperature), which can be either the glass transition (T_g) or the melting temperature (T_m) of the materials. Singhal et al synthesized polyurethanes foams with shape memory effects for embolic biomedical applications.

The usage of polyurethanes as SMPs suffers from several challenges such as thermal degradation, hydrolytic degradation, low stiffness and a dimensional instability after processing leading to the insufficient recovery stress, long recovery time and in some cases low value of shape fixity. The low stiffness of SMPUs results in a relatively small recovery force under constraint (actuation force) compared to alternative active actuation materials or schemes. Thus, in some applications, SMPUs may not generate sufficient recovery force to be viable. This drawback can be overcome by use of high modulus organic or inorganic fillers such as glass fibers, ceramic filler, poly (D,L-lactide), silsesquioxanes, celite, carbon nanotubes, carbon nanofibers, cellulose nanofibers and nanoclay particles to the polymer matrix.

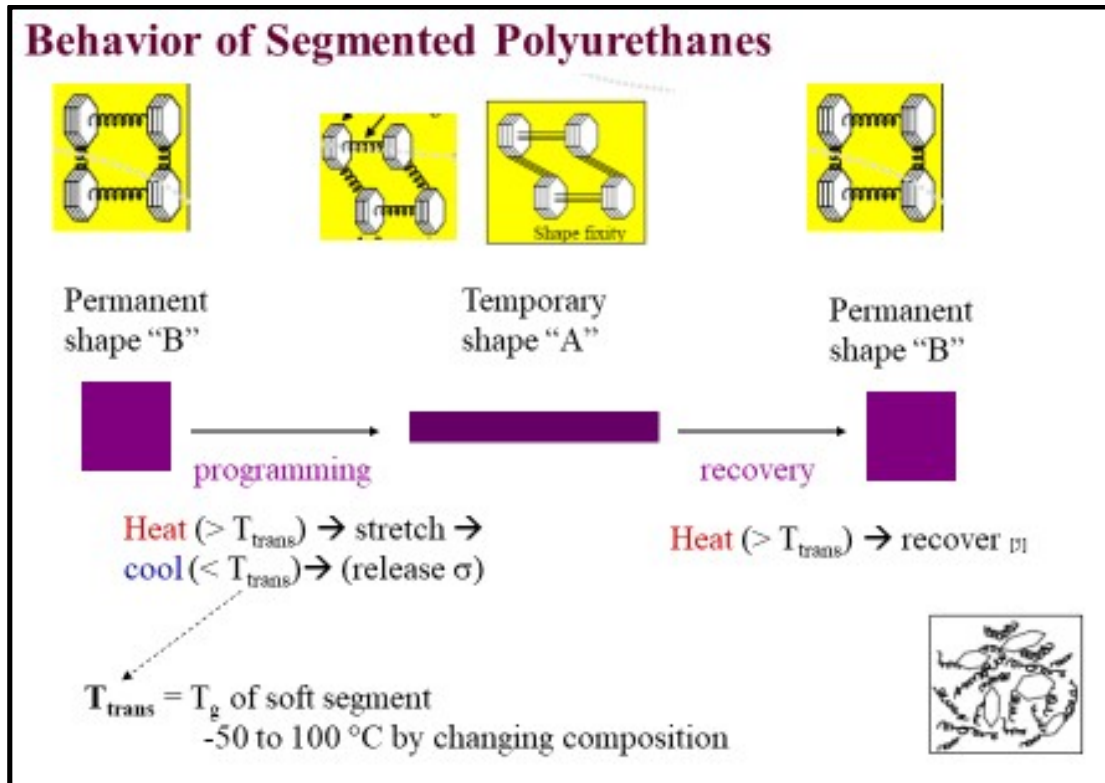


Figure 3. Behavior of shape memory polymers

Although shape memory polyurethanes have found extensive applications in biomedical field, but limitations like relatively low recovery stress, which is usually 1–3 MPa compared to 0.5–1 GPa for shape memory metal alloys [23-25], prevent their widespread applications. The relatively low recovery stress becomes a limiting factor in many applications especially in cases where a large resisting stress during shape recovery is required. One of the best avenue to improve mechanical properties and to add multiple functionalities to the shape memory polyurethanes is to mix with high modulus fillers [26] like carbon nanotubes, clays and cellulose nanofibrils. However, it has been observed that there is a trade-off between modulus enhancement and recoverable strain ratio due to the effects of filler particle size, much higher stiffness of fillers, or potential infringement with the polymer networks especially at high filler loadings. These issues can be alleviated by reducing the size of filler and the loading content which reduces the soft segment crystallinity. The reduction of soft segment crystallinity causes an imbalance of Helmholtz free energy, which in turn, caused a reduction of SM properties [27]. Chopped and continuous, especially continuous, nanofibres are superior to nano-sized particles to improve the mechanical strength of shape memory polymers [28]. The use of cellulose

nanofibers in segmented polyurethane matrix may be advantageous over traditional fillers because of the strong interactions that are formed between adjacent nanofibrils due to the surface hydroxyl groups, high stiffness of nanofibrils that improves the stiffness and strength of polymer matrix, increased thermal stability [29, 30] and decreased thermal expansion [31] of the resulting nanocomposite. At the same time, if a transparent matrix is used, it is possible to maintain most of the transparency due to the fine scale of the fibrils, even at fiber contents as high as 70% with an added advantage of low cost and renewability [32-34]. Well established procedure will be used to isolate cellulose nanofibrils from biomass using steam explosion method to get fibers of diameter range 4-50 nm and length 200-250 nm [35].

2. EXPERIMENTAL

2.1. Fourier Transform Infrared Spectroscopy (FTIR)

The chemical structure of lignin obtained at various pH values and alkali concentrations, lignopolyol, lignopolyol based polyurethanes, cellulose microfibrils (CMF), cellulose nanofibrils (CNF) and polyurethane/cellulose nanofibrils (PU-CNF) based nanocomposites (NPU) film was characterized by Fourier Transform Infrared Spectroscopy (FTIR) in Perkin Elmer model RZX-FTIR spectrophotometer (figure 5) using KBr technology i.e. by making pellets with KBr. FTIR spectra were recorded in a spectral range of 4000–450 cm^{-1} with a resolution of 2 cm^{-1} with two scans for each sample.

The relative level of cross linking in lignin can be calculated by absorbance ratios of peaks at 1500 and 1600 cm^{-1} [130]. The higher is the ratio more condensed and cross linked is the lignin.

S/G ratio for lignin was calculated by the estimating the intensities of the bands around 1327 cm^{-1} (S units) and 1271 cm^{-1} (G units), after resolution enhancement (subtraction of $\times 1000$ second derivative), moving-average smoothing ($\times 100$) and baseline correction between valleys ca. 1401 and 1172 cm^{-1} [131].

2.2. ^1H NMR

The chemical structure of castor oil was studied using Nuclear Magnetic Resonance (NMR) spectrometry. ^1H NMR spectra were recorded on a Bruker AV II 400 MHz spectrophotometer (figure 5). The ^1H NMR spectrum was obtained at 400 MHz using 10 mg acid-insoluble lignin and castor oil/ polyol in 0.5 mL of dimethylsulfoxide- d_6 (DMSO- d_6). The chemical shifts of ^1H NMR spectrum were calibrated with reference to DMSO, used as an internal standard, at 2.49 ppm. The acquisition time was 2.7 s, and relaxation time was 1.0 s.

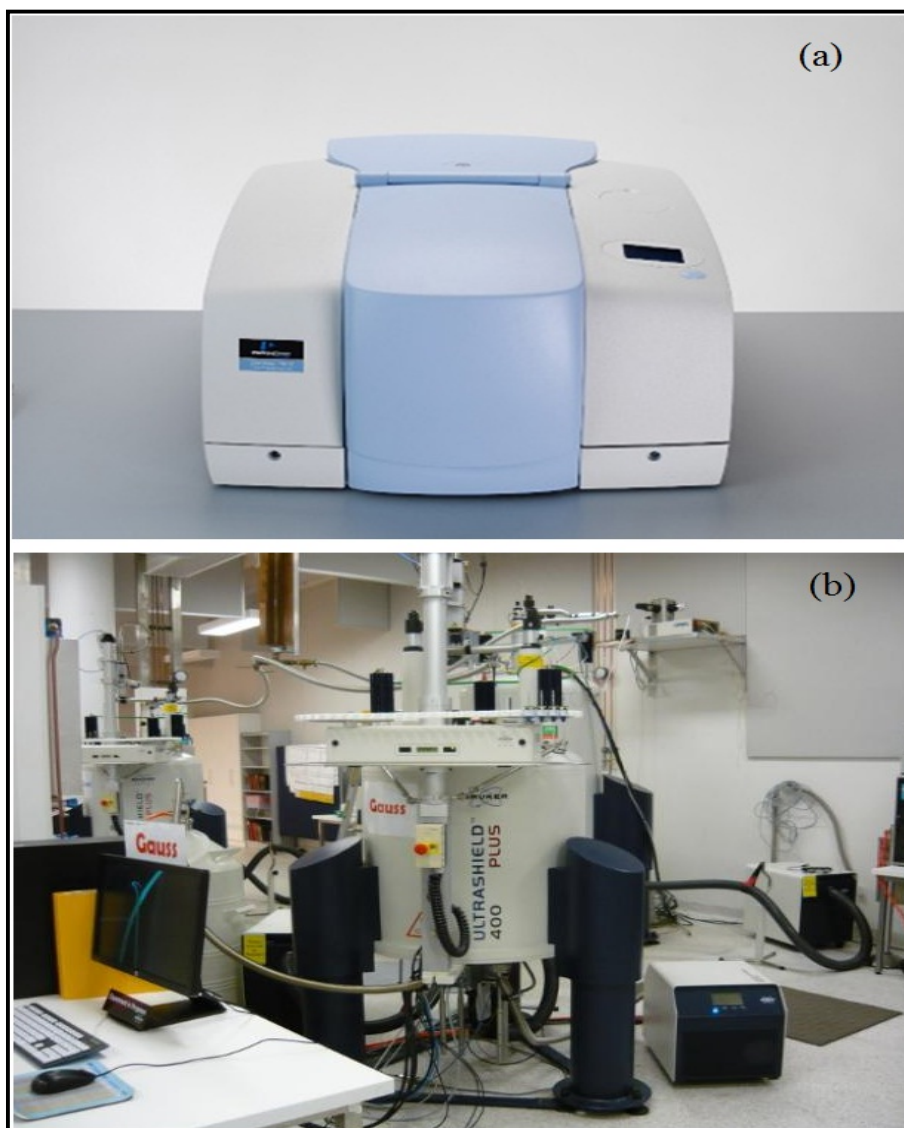


Figure 5: Photographic images of (a) Perkin elmer model RZX-FTIR spectrophotometer; (b) Bruker AV II 400 MHz NMR spectrophotometer

2.1. UV-Vis Spectrophotometer

UV-vis spectrophotometer is used to study the chemical structure and purity of lignin. For this a Shimadzu spectrophotometer model UV-1200 (figure 6) was used. Prior to the analysis, 5mg of sample was dissolved into 10 ml 90% (v/v) dioxane-water aliquot. 1 ml of aliquot was further diluted into 25 ml by using 50% (v/v) dioxane-water. The absorbance was measured for the range of 200 nm to 400 nm [189].

2.2. Elemental Analysis (C, H, N AND O)

Elemental analysis (C, H, and N) was performed on lignin, castor oil/ polyol, CMF and CNF samples using Thermo Finnigan Elemental Analyzer (figure 6) for CHN and the Oxygen content were calculated by difference. Prior to analysis samples were vacuum dried at 100⁰C overnight, to remove traces of moisture.



Figure 6: Photographic images of (a) Shimadzu spectrophotometer model UV-1200; (b) Thermo Finnigan Elemental Analyzer

2.3. Estimation of Hydroxyl Value

The hydroxyl value is defined as the number of milligrams of potassium hydroxide equivalent to the hydroxyl content of one gram of the sample.

In spite of the numerous techniques that have been reported in the literature [374–377] for the determination of hydroxyl content, most widely used method is Phthalation and Acetylation. The

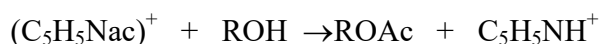
second method involves acetylating the sample with acetic anhydride in pyridine (as solvent) and excess anhydride is estimated by titrating with alcoholic potassium hydroxide after it has been decomposed with water to generate acetic acid.

Different ratios of acetic anhydride in pyridine have been recommended. The ratios are important since they affect reaction time and therefore quantitative results. The total number of hydroxyl groups that can be quantitatively acetylated with a given volume of reagent and the ratios also have some effect on quantitative accuracy. The type and amounts of hydroxyl groups, such as primary and secondary hydroxyl groups also influence accuracy since they do not acetylate with same ease. Generally 1:3 ratio of acetic anhydride to pyridine is used.

The proposed mechanism for the catalyzed acetylation in pyridine is:



The pyridine acetylium ion then reacts with the alcohol to form ester and regenerate the pyridinium ion.



For estimation, a known quantity of dried sample was taken in an Erlenmeyer flask 10ml of acetylating reagent (containing 1:3 ratios of acetic anhydride and pyridine) was added, along with some pieces of non-porous (Carborundum) boiling chips or pumic stone. An air condenser was fixed vertically in the neck of the flask and heated to slow boil in water bath for one hour. Then the mixture was allowed to cool a bit, and 5 ml distilled water was added for decomposition of excess acetic anhydride. It was finally heated for 10-15 minutes more to ensure complete decomposition of acetic anhydride. On cooling, sides of the condenser were washed with little more water and the contents titrated as a whole against 1N standard alcoholic potassium hydroxide solution using phenolphthalein indicator. A blank experiment was also run simultaneously under same conditions. The hydroxyl value was calculated as:

$$OH_{No.} = \frac{56.1 \times N_{NaOH} \times (ml_{blank} - ml_{sample})}{weight\ of\ sample} \times 100 \quad (2.3)$$

2.4. MALDI-Time-of-Flight Mass Spectrometry(MALDI-ToF)

Mass spectra of lignin and castor oil/ polyol was recorded on an Autoflex III MALDI time-of-flight mass spectrometer of BrukerDaltonics (figure 7) operating in the reflector and linear

positive or negative mode using a pulsed nitrogen laser (1337 nm, pulse rate of 10 Hz) as the ionization source. The analyzer was used at an acceleration voltage of ± 20 kV. Laser light was focused on the sample using a 5.2 kV lens. A pulsed ion extraction was optimized to 200 ns. Lignin samples were dissolved in dimethylformamide (DMF) with a concentration of 10 mg/mL and DHB (2, 5-dihydroxybenzoic acid) used as matrix material was also dissolved in DMF. Overall, 2 μ L of lignin and 2 μ L of matrix were mixed together in a plate. 1 μ L of sample was deposited on each well of the stainless steel multiple sample container and permitted to dry in air. The sample was completely dried in air before introducing in the mass spectrometer. A peptide calibration set was used as an external standard. A total of 300 shots were provided. Each sample preparation and analysis was duplicated.

Weight average molecular weight, number average molecular weight and polydispersity index of the EL and ML was calculated using equation 2.4 to 2.6 [378]:

$$M_n = \frac{\sum(N_i M_i)}{\sum N_i} \quad (2.4)$$

$$M_w = \frac{\sum(N_i M_i^2)}{\sum(N_i M_i)} \quad (2.5)$$

$$P_i = \frac{M_w}{M_n} \quad (2.6)$$

Where, M_n = Number average molecular weight.

M_w = Weight average molecular weight

N_i = Signal intensity of the i^{th} oligomers in the distribution.

M_i = Molecular weight of i^{th} oligomers in the distribution

P_i = Polydispersity Index

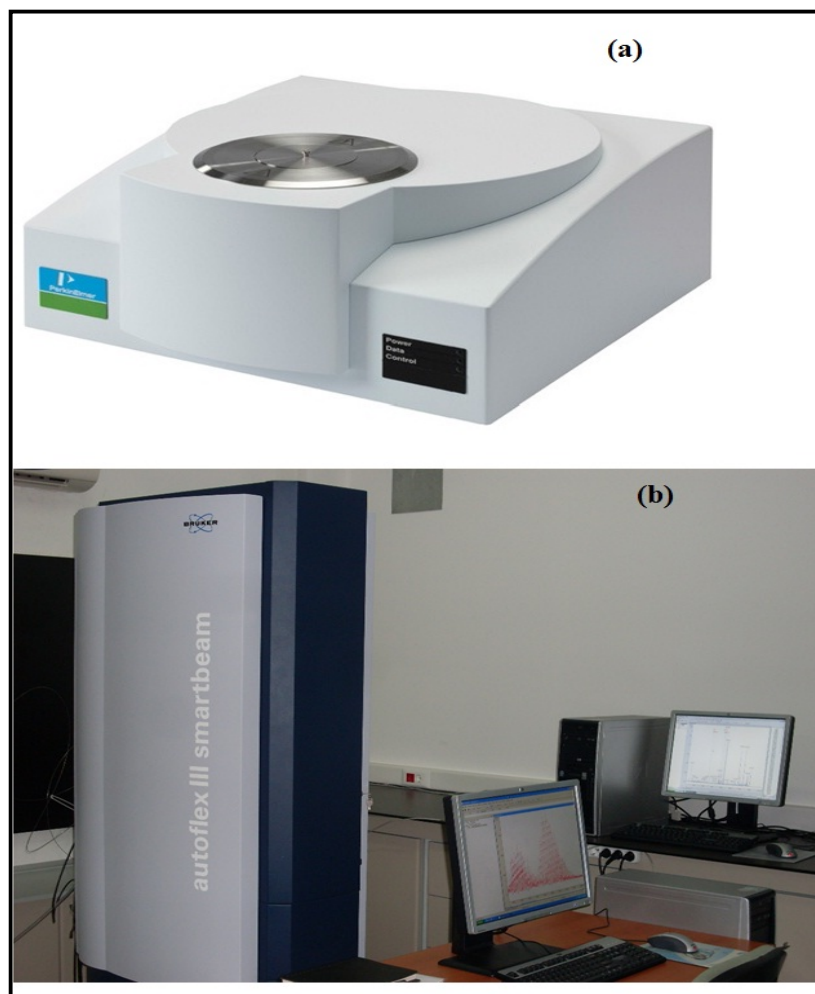


Figure 7: Photographic images of (a) Thermo gravimetric Analyzer (TGA) of Perkin Elmer STA-6000; (b) Autoflex III MALDI time-of-flight mass spectrometer of BrukerDaltonics

2.5. Thermal Gravimetric Analysis (TGA)

Thermal stability of lignin, castor oil/ polyol, castor oil/ polyol based polyurethanes, CMF, CNF and PU/CNF nanocomposites films was studied using a Thermo gravimetric Analyzer (TGA) of type Perkin Elmer STA-6000 (figure 7). Approximately 10 mg of sample was weighed in an aluminum pan and placed in thermo gravimetric analyzer (TGA). Heating was done at a rate of $10^{\circ}\text{C min}^{-1}$ from room temperature to 800°C in nitrogen atmosphere at a flow rate of 15mL min^{-1} . Percent weight loss was plotted against temperature. A derivative of this curve, DTG was obtained to indicate the temperatures at which maximum rates of weight loss occurred.

2.6. Scanning Electron Microscopy (SEM)

Scanning Electron Microscope (SEM) model JSM JEOL-6490 (figure 8) was used for morphological analysis of lignin, castor oil/ polyol, castor oil/ polyol based polyurethanes CMF and PU/CNF nanocomposites films. For these analysis, all samples were mounted on a metal stub and platinum coated by using sputter coating technique for 20 s to make them conducting. Images were taken at 20 kV accelerating voltage at different magnifications.

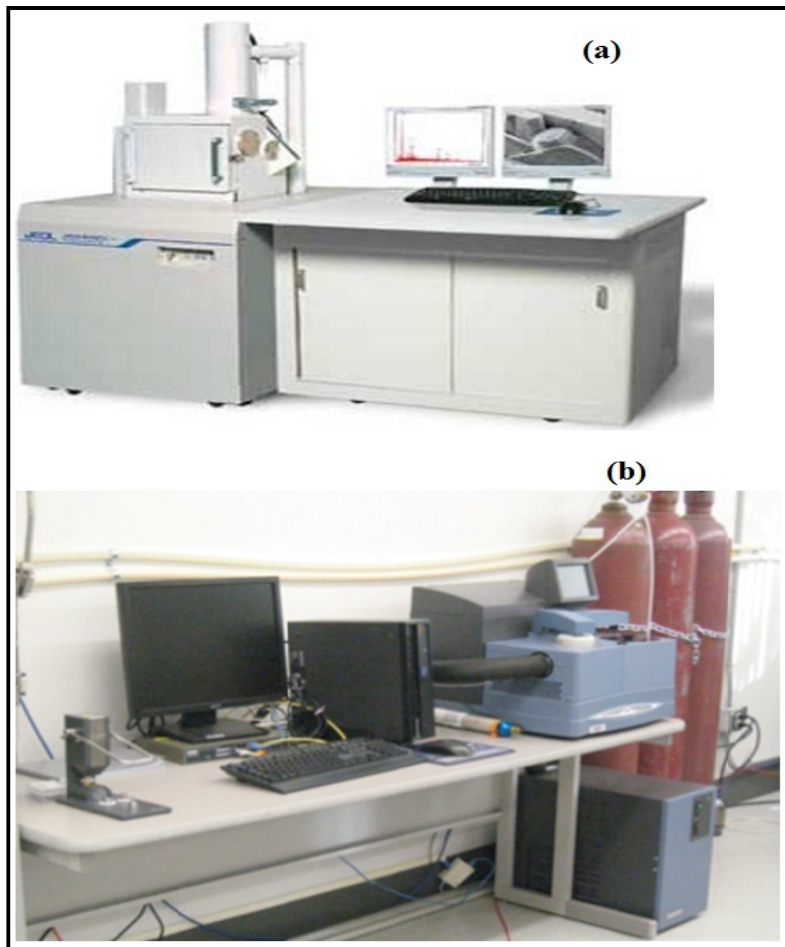


Figure 8: Photographic images of (a) SEM model JSM JEOL-6490; (b) DSC from TA Instruments Inc model no. Q2000

2.7. Differential Scanning Calorimeter (DSC)

DSC measurements of lignin castor oil/ polyol, castor oil/ polyol based polyurethanes, CMF, CNF and PU/CNF nanocomposites films were performed using Q2000 from TA Instruments Inc (figure 2.9 b). Approximately 5.0 ± 0.25 mg samples were placed in a hermetic pan and

sealed. DSC scans were performed at a heating rate of 10°C/min from 30 to 400°C under nitrogen environment.

2.8. Transmission Electron Microscopy (TEM)

The network and surface topography of cellulose nanofibers was observed using Transmission Electron Microscopy (TEM) model Hitachi-2100 (figure 9). All the images were taken at 80 kV accelerating voltage. The sample for the test was prepared by depositing and drying a drop of dilute NFC suspension (prepared in de-ionized water) on a carbon coated grid.

The diameter and length of CNF were examined using TEM images of nanofibers. For this, TEM images of NFCs were loaded in UTHSCSA Image Tool analyzer program (IT version 3) and diameters of the fibers were measured using a two point measuring analysis. The scale of the software was calibrated using the scale bars on each TEM image. Approximately 300 measurements were taken to obtain fiber diameter distribution.



Figure 9: Photographic image Transmission Electron Microscope (TEM)

2.9. Wide Angle X-Ray Diffraction (WAXRD)

WAXRD of castor oil/ polyol based polyurethanes film, CMF, CNF and PU/CNF nanocomposites film was conducted by subjecting the samples to X-ray radiation at room temperature. The films were analyzed by using a Philips X'Pert Pro R-ray diffractometer system (figure 10). The radiation was Cu K α ($\lambda=1.54060 \text{ \AA}$) with 40 kV voltage and 40 mA intensity.

Crystallinity and crystallite size of the raw jute fibers, CMF, CNF was calculated using the following equations:

$$\text{Crystallinity Index (CrI)} = 100 \times \frac{I_{Total} - I_{Am}}{I_{Total}} \quad (2.7)$$

Where, I_{Total} is the maximum intensity of the (002) lattice diffraction and I_{Am} is the intensity diffraction at $18^\circ 2\theta$ diffraction angle.

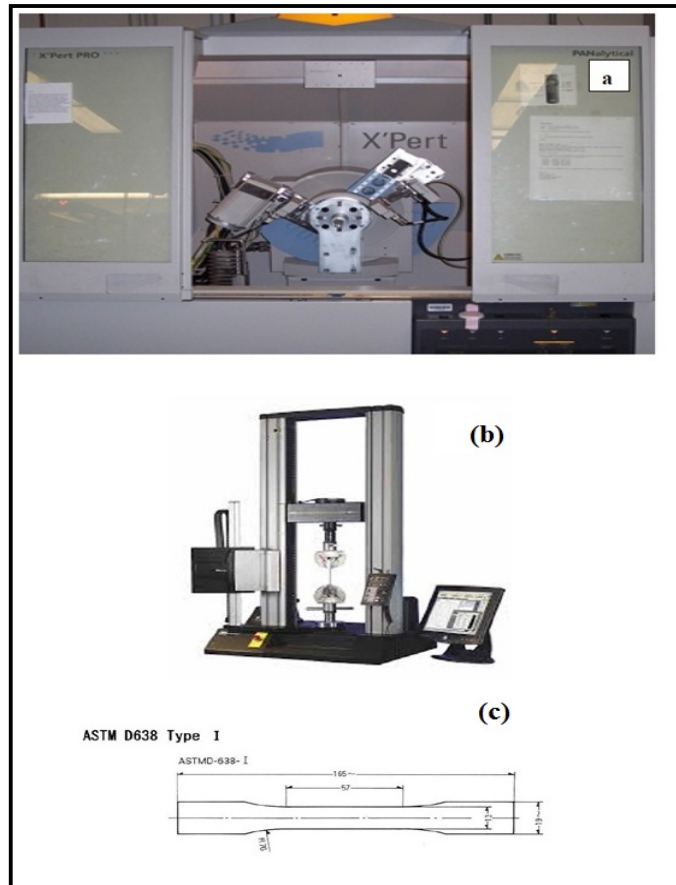


Figure 10: Photographic images of (a) X'PertPro X-ray diffractometer system; (b) and (c) Instron 4466 instrument; sample shape and its dimensions as per ASTM D638 standard

The crystallite size or the thickness of crystal in a direction perpendicular to its Miller planes was also estimated using Scherer's equation (2.8)

$$t_{hkl} = \frac{K\lambda}{\beta_{hkl}\cos\theta} \quad (2.8)$$

Where, t_{hkl} is taken as the thickness of crystallites at the (hkl) plane of diffraction, λ is an X-ray wavelength ($\lambda = 0.1542$ nm for CuK α), θ is the Bragg angle of the reflection, β_{hkl} is the pure integral of width of the reflection at half maximum height, and K is the Scherrer constant that falls in the range 0.87-1.0.

2.10. Mechanical Analysis

Tensile testing of castor oil/ polyol based polyurethane samples and PU/CNF nanocomposite films was done using Universal Tensile Testing machine Instron 4466 (figure 2.11 b) upgraded with Blue Hill 2 software and assembly A564-229 version 2.0. The load cell of 10 kN was installed following ASTM D638 standards. For the test, crosshead speed was set to 2 mm/min and film samples were cut in a dumbbell shape (figure 10). Four to five specimens were tested for each sample and average value was taken. A stress vs. % strain curve was obtained from which the tensile strength and yield strength of castor oil/ polyol based polyurethanes films was calculated.

2.11. Antimicrobial Activity (Growth Conditions and Inhibition Analysis)

Antimicrobial activity of PU/CNF nanocomposites was examined by macrodilution method against *Staphylococcus aureus* (Gram-positive) and *Escherichia coli* (Gram-negative). For this the bacterial strains were grown overnight in Brain heart infusion broth at 37°C and 100 μ l of culture was added to the freshly prepared 10 ml Mueller hinton broth containing castor oil/ polyol based polyurethanes sheets (5 mm x 5 mm). PU/CNF nanocomposites free broth served as control. Inhibition of bacterial growth was visible as a clear broth and the presence of growth was detected by the presence of turbidity. Further, overnight growth was also monitored by measuring the optical density at 600 nm.

2.12. Biodegradation Study in PBS Solution

The PU/CNF nanocomposites films of about 10 x 10 mm² with weight ' W_o ' were placed in a beaker with 25 mL of a PBS buffer solution with pH=7.4 and then incubated at 37°C. At specific time intervals, the specimen was taken out, washed with double distilled water and kept for

drying in vacuum oven for 2 days till constant weight was achieved. Then final dried weight (W_d) was determined. % Degradation was evaluated using Eq. (2.9):

$$\% \text{ Degradation} = \frac{(W_o - W_d)}{W_o} \times 100 \quad (2.9)$$

3. RESULTS AND DISCUSSION

Characterizations of Cellulose Nanofibers

Cellulose nanofibers were isolated using physical-chemical methods followed by high shear homogenization. The overall isolation of cellulose nanofibrils is a two-step process involving:

- i. Extraction of cellulose micro fibers (CMF) aggregates using soda cooking and bleaching followed by acid hydrolysis of the raw jute fibers.
- ii. Mechanical disintegration of microscopic cellulose fibers (CMF) aggregates into nanofibrillated cellulose (CNFs) using high shear homogenization.

Soda cooking, the first and the primary step which results in the defibrillation of large cellulose bundles in to microscopic cellulose fibers (CMF) with the removal of all the components like lignin, hemicelluloses, pectin leaving pristine cellulose. Microscopic cellulose fibers (CMF) aggregates in the second step are mechanically disintegrated into nanofibrillated cellulose (CNFs).

This section deals with the morphological, structural and thermal characterizations of raw jute fibers, microscopic cellulose fibers (CMF) and nanofibrillated cellulose (CNFs). The various analytical techniques like TEM, SEM, FT-IR, XRD, TGA DSC and elemental analysis were used at different stages of the isolation.

Yield of Cellulose Microfibers and Cellulose Nanofibers

Yield of the cellulose microfibers (CMF) and cellulose nanofibers (CNF) was calculated using equation 2.2 and found to be 55 and 53%, respectively. There was a slight decrease of 2% in the yield of cellulose nanofibers that may be due to wastage during processing of cellulose microfibers.

Fourier Transform Infrared Spectroscopic Analysis (FTIR)

Traces of lignin, hemicelluloses and pure cellulosic groups present in raw jute fibers, microscopic cellulose fibers (CMF) and nanofibrillated cellulose (CNFs) were identified using FTIR spectroscopy technique. Figure 11 shows the FTIR spectra of raw jute fibers, chemically treated microfibrils (CMF) and mechanically treated cellulose nanofibrils (CNF), while table 3.1 shows the prominent peaks of these spectra and their description.

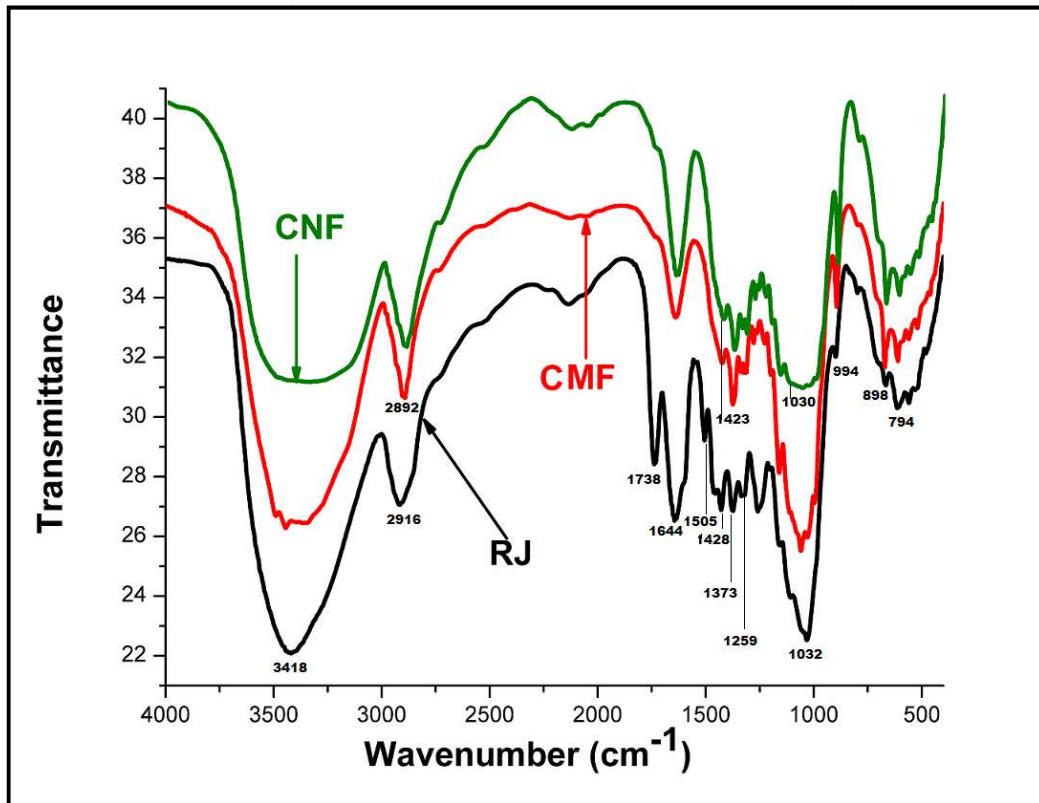


Figure 11: FTIR spectra of Raw Jute raw jute fibers, chemically treated microfibrils (CMF) and mechanically shear treated cellulose nanofibrils (CNF)

In the FTIR spectra a broad peak in the range of 3,200–3,500 cm^{-1} was due to O–H stretching vibration and bands at 2850–2930 cm^{-1} were due to methyl and methylene groups. Peak at 1732 cm^{-1} in the spectrum of raw jute fibers is either due to the acetyl and uronic ester groups of the hemicelluloses or the ester linkage of carboxylic group of the ferulic and p-coumaric acids of lignin and/or hemicelluloses. Bands around 1652 cm^{-1} maybe due to the bending mode of the absorbed water and some contributions from carboxylate groups. The strong and sharp band around 897 cm^{-1} and 655 cm^{-1} corresponds to C-H deformation ring vibrations and C-OH out-of-plane, respectively. Bands at 1510 and 1425 cm^{-1} correspond to aromatic ring vibrations of

phenyl propane groups of lignin seen in spectrum of raw jute whereas in case of chemically treated fibers the band around 1510 cm^{-1} vanished completely. The intensity of peak at 1426 cm^{-1} has significantly decreased in chemically treated fibers attributing to partial removal of lignin. The peak at 1373 cm^{-1} represents C-H asymmetric deformation seen in all the spectra whereas the peak at 1258 cm^{-1} corresponds to hemicelluloses which diminished completely in case of chemically and mechanically treated fibers thus indicating the complete removal of hemicellulose. Peak at 895 cm^{-1} in chemically and mechanically treated fibers relates to the crystalline regions of cellulose associated with cellulosic β -glycosidic linkages.

Table 1: Observed peaks with their band description for Raw Jute raw jute fibers, chemically treated microfibers (CMF) and mechanically shear treated cellulose nanofibers(CNF)

Band Description	Observed peaks/bands		
	RJ	CMF	CNF
-OH Stretching	3418	3366	3335
C-H Vibration	2916	2892	2892
C=O stretching due to hemicellulose	1738	-	-
Absorbed water	1644	1639	1644
Aromatic C=C vibration of lignin	1609	-	-
	1505	-	-
	1428	1423	1423
C-H stretching	1373	1373	1373
Hemicellulose	1259	-	-
C-O-C stretching	1163	1160	1160
C-C stretching	1032	1031	1030
C-H Rock vibration of cellulose	994	996	996

	898	894	894
	794	796	-

Wide Angle X-Ray Diffraction (WAXRD) Analysis

WAXRD analysis is performed for studying the crystalline behavior and for determining structure-property relation of the fibers. In all natural fibers, cellulose is highly crystalline by nature but its binding components lignin, hemicellulose and other components are amorphous which results in decrease in overall crystallinity of the natural fibers. Hence, the crystallinity of fibers is enhanced after chemical treatments as it removes lignin and other components [66,306]. Figure 12 shows the XRD patterns of raw jute fibers, CMFs and CNFs. From the XRD patterns, it was inferred that the chemical treatment resulted in the transformation of native cellulose I to cellulose II. It can be confirmed from the shifting of peak from 16.8° to 12.5° 2θ angle and evolution of new peak at 2θ 20.5° corresponding to cellulose II. It may be due to penetration of liquor in cellulose fibers during soda cooking causing a rearrangement of the crystal packing of chains from native cellulose I to cellulose II. Also a sharp intensity peak for native cellulose I was observed at 22.6° thus confirming the coalescence of cellulose I and II. The nanostructure obtained resulted in increase in specific surface area of the fiber, making the hydroxyl groups of cellulose macromolecules more accessible. Similar results were observed for CNF. From figure 12 it was also observed that crystallinity of fibers increased with the chemical treatment as indicated by increase in the intensity of peak at $2\theta = 22.6^\circ$ corresponding to 002 lattice plane and further increases sharply with high shear mechanical treatment.

Table 2 shows that the crystallinity and crystallite size of raw jute fibers, CMF and CNF. The crystallite size decreased from 13.57 nm for chemically treated to 2.84 nm for cellulose nanofibers whereas crystallinity increase from 44.99% for untreated to 94% for mechanically/high shear treated cellulose nanofibers. This increase in crystallinity could also be attributed to reorganization of amorphous and para-crystalline region of cellulose at higher temperature during soda cooking process which may have accumulated during the crystallization

phase of cellulose biosynthesis and interaction of the cellulose with hemicellulose and lignin in cell wall formation.

Table 2: Crystallinity and crystallite size Raw Jute raw jute fibers, chemically treated microfibrils (CMF) and mechanically shear treated cellulose nanofibrils (CNF)

Sample ID	% Crystallinity	Crystallite Size
RJX	45	-
MFC	84	13.57
CNF	98	2.48

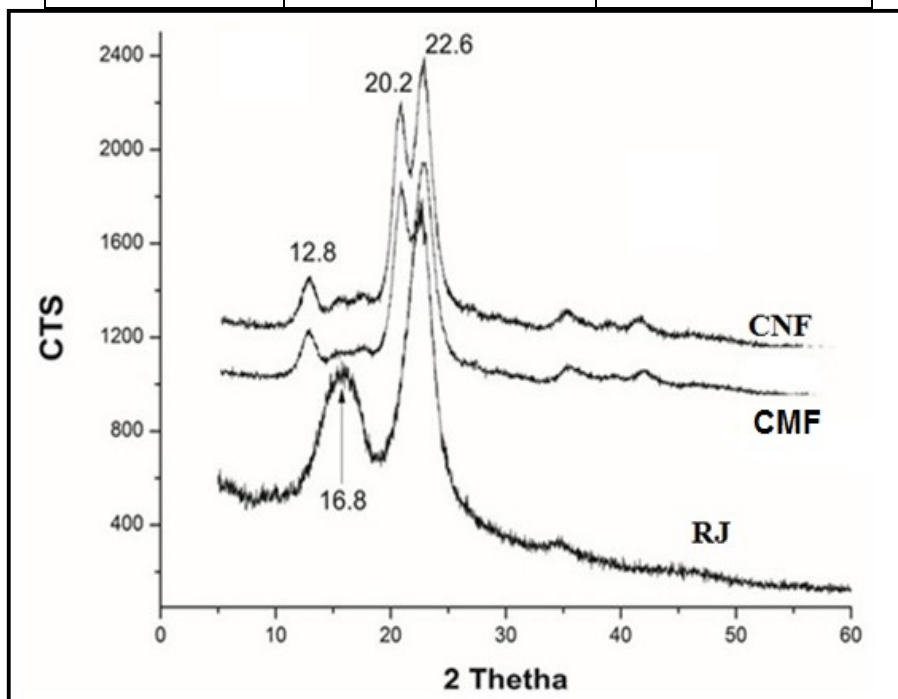


Figure 12: XRD patterns of Raw Jute raw jute fibers, chemically treated Microfibrils (CMF) and mechanically shear treated cellulose nanofibrils (CNF)

Scanning Electron Microscope (SEM)

Scanning electron microscopic images of raw jute fibers and chemically treated microfibrils CMF obtained after acid hydrolysis were taken to determine the microstructure of cellulosic

fibers. Structural as well as chemical changes were observed after soda cooking process as it results in the fragmentation of bonds of lignin, hemicellulose in the cell wall.

Surface morphology of raw jute fibers and chemically treated CMFs are shown in Figure 13(i) and 13 (ii) at different magnifications, respectively. SEM micrographs shown in Figure 13 (ii) (a-d), clearly show individual fibers with an average diameters of about 10–15 μm , lower than the average size of fiber bundles which get disrupted with the removal of hemicelluloses, lignin, and pectin during chemical treatment. This reduction of size may be attributed to the disintegration of hemicellulose and lignin corroborated by FTIR results. SEM images also show that the obtained fibers are cylindrical in shape. Further, SEM images clearly show the effect of physicochemical treatments i.e. soda cooking, bleaching and acid hydrolysis. Isolation of cellulose microfibrils bundles that are major component of ligno-cellulosic material was also confirmed from SEM images.

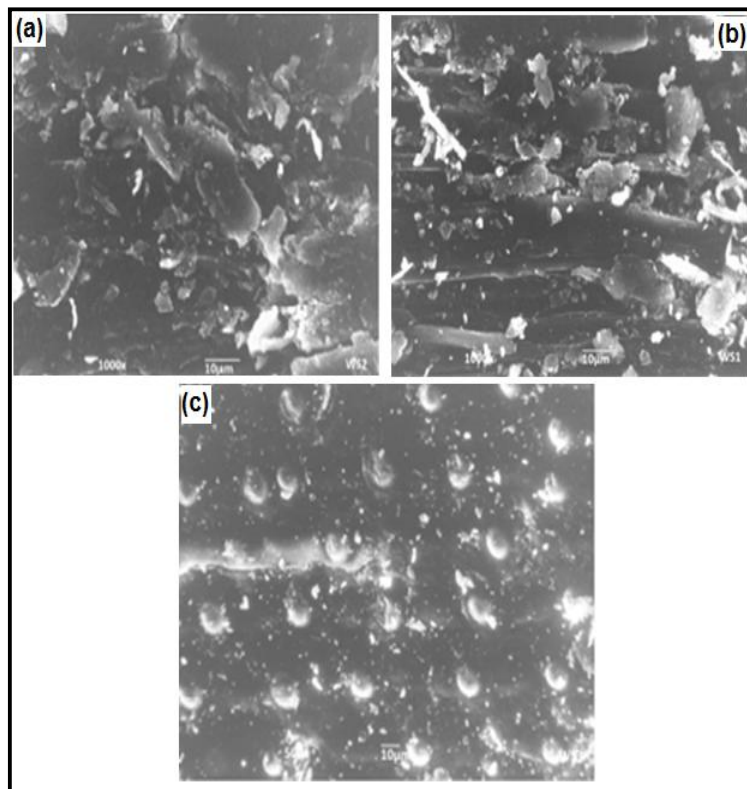


Figure 13 (i): SEM images of Raw Jute fibers at different magnifications

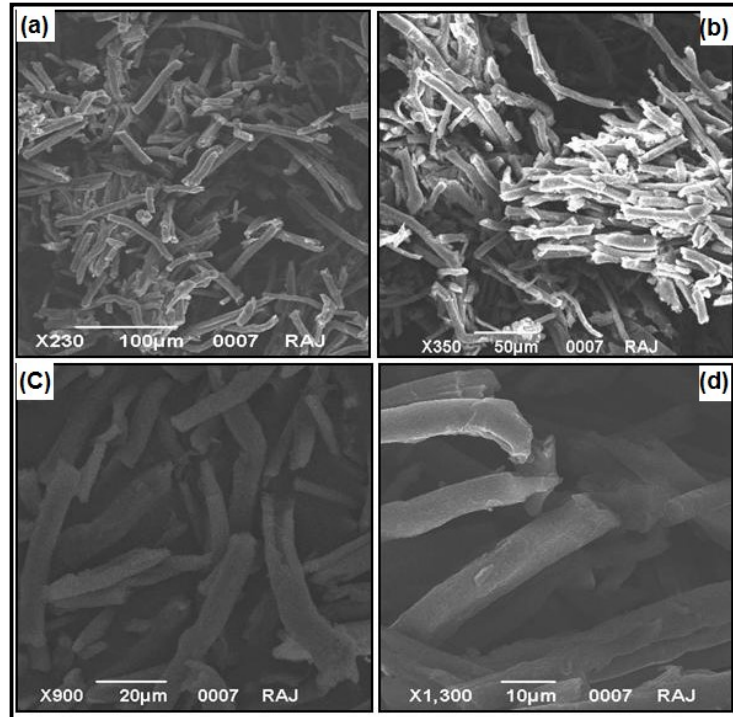


Figure 13 (ii): SEM images of chemically treated cellulose microfibrils (CMFs) at different magnifications

Transmission Electron Microscope (TEM)

Figure 14(i) shows TEM images of the CNFs after the chemical and mechanical treatments. Mechanical treatment resulted in defibrillation of the cellulose nanofibrils from the cell bundle and thus TEM images reveal the disintegrated nanofibers from the micro sizes fiber bundles. The diameter of the fibers was found in the range of 5–60 nm. A tendency of agglomeration can also be observed in TEM images. It is not clear whether this was due to drying of the suspension onto the carbon film covering the carbon grids or if it reflected the state of the suspension.

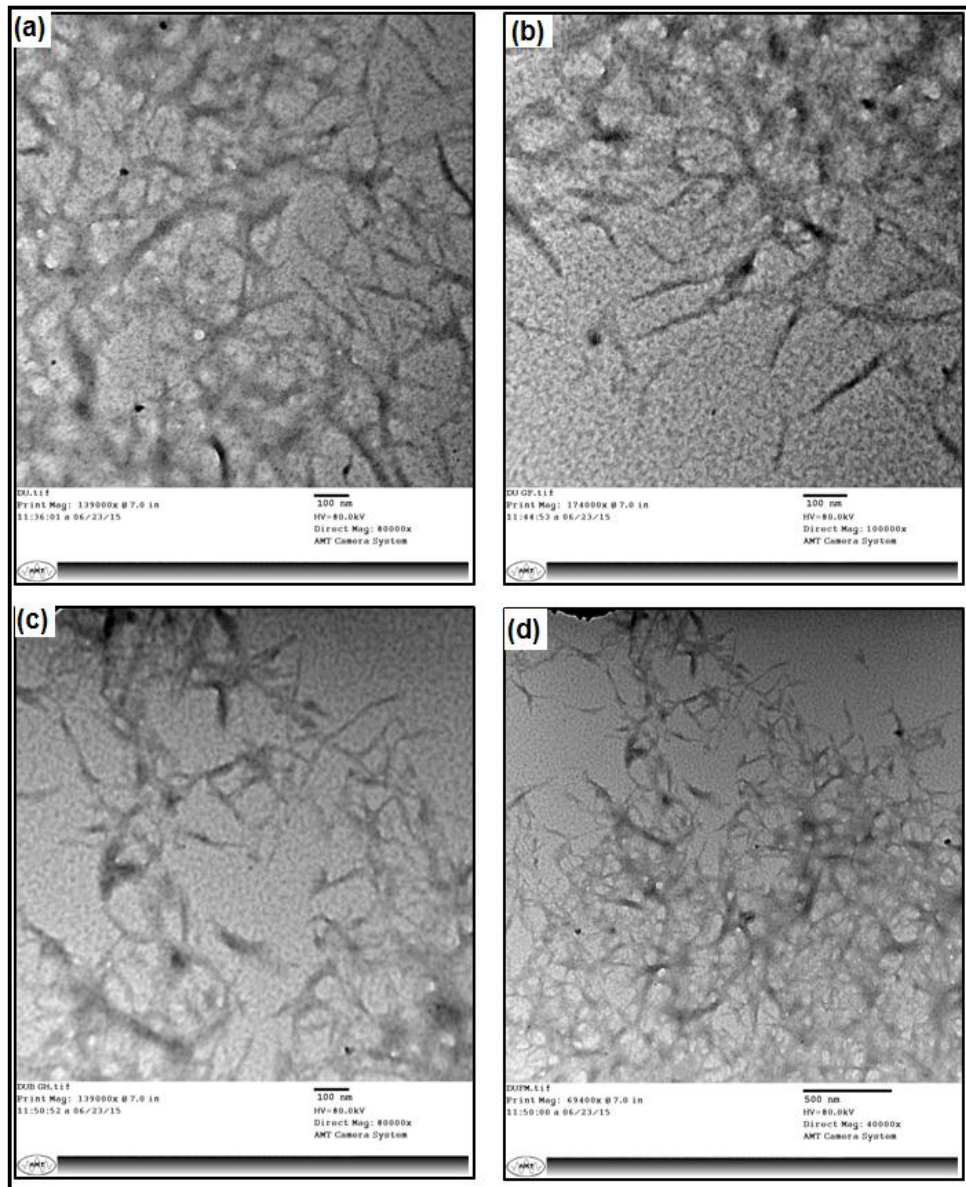


Figure 14 (i) a-d: TEM images of mechanically treated cellulose nano fibers (CNFs) at different magnifications

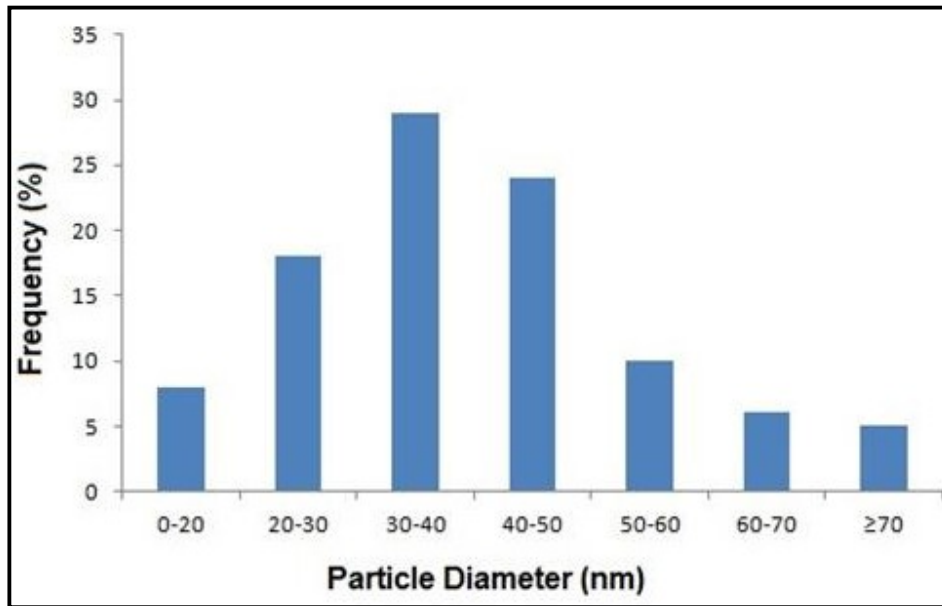


Figure 14(ii). Particle size distribution using image tool analyzer (UTHSCSA).

UTHSCSA digital image analysis software was used to calculate the average diameter from the electron micrographs. Diameter was found to be in the range of 30–50 nm for most of the particles. Figure 14(ii) shows the distribution of nanofibers diameter after final treatment from which it was revealed that only 5% of fibers have diameter >70 nm. Almost 62% of fibers have diameter between 30–50 nm and 18% of the fibers have a diameter less than 30 nm.

Thermal Analysis of Raw, Chemically (CMFs) and Mechanically (CNFs) treated Jute Fibers

The main objective behind isolation of cellulose nanofibers is to synthesize polyurethane nanocomposites by reinforcing them into polyurethane matrix. It also gives an idea about purity of cellulose. Therefore, thermal analysis of nanofibrils becomes important for their processing. TGA curves gives information about the percentage weight loss with respect to temperature while (DTG) demonstrate the corresponding rate of weight loss. The point at which maximum rate of thermal decomposition occurs is predicted from the peak of DTG curves and is termed as DTG_{max} and is used for comparing thermal stability of various samples.

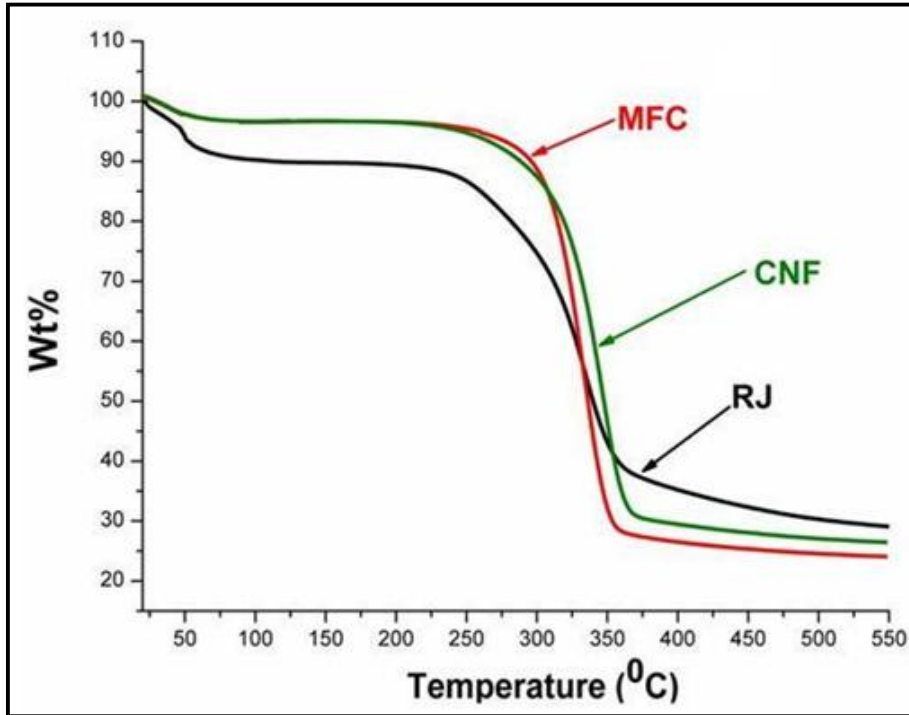


Figure 15 (i): TGA curves of Raw Jute raw jute fibers, chemically treated Microfibers (CMF) and mechanically shear treated cellulose nanofibers (CNF)

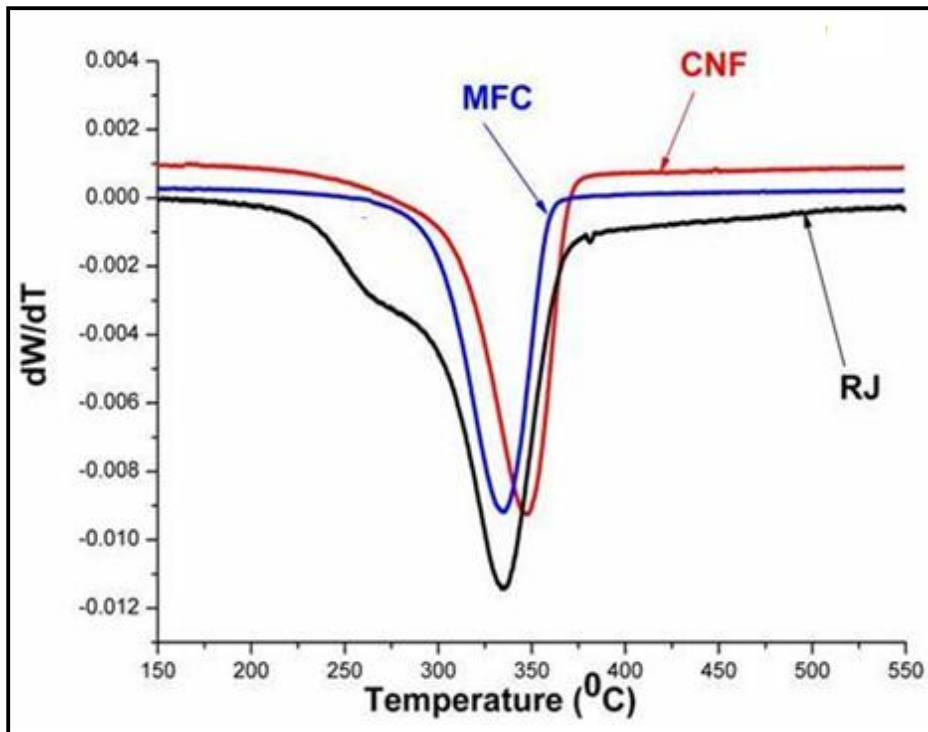


Figure 15 (ii): DTGA curves of Raw Jute raw jute fibers, chemically treated Microfibers (CMF) and mechanically shear treated cellulose nanofibers (CNF)

TGA and DTG curve of raw jute fibers, CMFs and CNFs are shown in figures 15(i) and 15(ii), respectively. From the TGA of raw jute, it is apparent that degradation occurs between a broad range of 120 to 550°C. The initial weight loss around 100°C was due to the evaporation of absorbed moisture. Second and third degradation stage at 230 and 350°C corresponds to degradation of hemicellulose and cellulose. The last stage of degradation above 370°C corresponds to degradation of lignin. It was observed that in case of chemically and mechanically treated fibers, the thermal stability T_{onset} is higher which may be due to complete removal of amorphous non-cellulosic material resulting in higher degree of ordered structure of crystalline cellulose.

From DTG results shown in figure 15(ii) three major degradation peaks were observed in case of raw jute. First decomposition shoulder peak at 250°C relates to the thermal depolymerization of hemicelluloses or pectin, the second major peak due to degradation of cellulose was seen at 338 °C and finally a small tail at 370 °C relates to the degradation of lignin. In case of chemically and mechanically treated fibers, only a sharp second peak around 335-350°C appears which corresponds to decomposition of highly crystalline cellulose, whereas 1st and 3rd peak disappeared showing the complete removal of lignin and hemicellulose as also confirmed from other results.

The thermal degradation characteristics like T_{onset} , T_{max} and their corresponding % mass loss and % mass residue at 550 °C of raw jute, CMFs and CNFs are tabulated in table 3. Where T_{onset} relates to the temperature at which degradation starts, T_{max} to the temperature where maximum degradation takes place. From the results, it was observed that the T_{onset} , T_{max} and % mass loss at T_{max} for CNFs is higher than raw jute fibers, confirming their higher thermal stability. The higher thermal stability of CNFs may be attributed either to the presence of organic compounds or may be due to complete removal of amorphous non cellulosic material resulting in higher degree of ordered structure of crystalline cellulose as substantiated by FTIR and XRD results.

Table 3: Thermal degradation characteristics of Raw Jute raw jute fibers, chemically treated microfibers (CMF) and mechanically shear treated cellulose nanofibers (CNF)

Sample ID	T_{onset} (°C)	%Mass loss at T_{onset}	T_{max} (°C)	%Mass loss at T_{max}	% Mass Residue at 550°C
-----------	------------------	---------------------------	----------------	-------------------------	-------------------------

RJ	288	23.70	332	42.62	29.30
CMF	300	15.59	340	58.17	15.44
CNF	311	18.13	348	64.68	11.94

Differential Scanning Calorimeter (DSC) is another important technique for the analysis of thermal properties. It provides important information regarding transition temperature i.e. the temperature at which the material morphology changes from crystalline to amorphous and about the degradation whether it is endothermic or exothermic.

DSC curves of raw jute fibers, MFCs and CNFs are shown in figure 16. From the figure a peak below 150°C is observed in case of raw, MFCs and CNFs, this may be due to the evaporation of moisture from the sample on heating. Further, in case of raw jute fibers, two more degradation peaks were seen in the range of 290-310°C and 340-360°C similar to TGA, that may be due to the degradation of hemicellulose and α -cellulose. However, in case MFCs and CNFs only one degradation around 320°C was observed corresponding to the degradation of crystalline cellulose which further reaffirms the observation of TGA results.

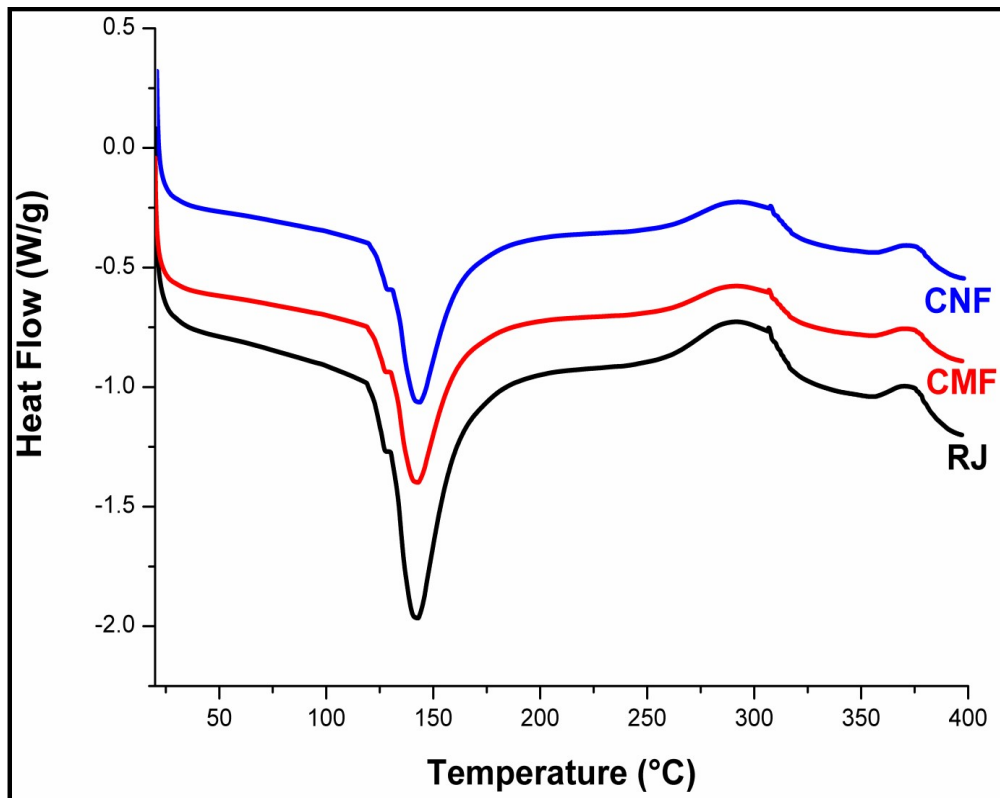


Figure 16: DSC curves of Raw Jute raw jute fibers, chemically treated Microfibers (CMF) and mechanically shear treated cellulose nanofibers (CNF)

Table 4: Degradation temperatures and their corresponding enthalpies from DSC results

Sample	First degradation temperature (°C)	Enthalpy at first degradation (J/g)	Second degradation temperature (°C)	Enthalpy at Second degradation (J/g)
CMF	137.47	82.03	348.14.	56.32
CNF	137.65	58.51	357.31	35.60

Elemental Analysis of Raw, chemically (CMFs) and mechanically (CNFs) treated fibers

The elemental analysis results i.e. C, H, O, N, S wt% and O/C and H/C ratios of the MFC and cellulose nanofibers (CNF) are shown in table 5.

Table 5: Elemental analysis depicting C, H, O, N, S wt%

Sample ID	%C	%H	%O	%N	%S	O/C	H/C
MFC	50.56	7.38	41.76	0	0	0.82	0.14
CNF	51.12	7.59	42.18	0	0	0.83	0.15

From the results, it is revealed that no sulphur was present in the chemically and mechanically treated fibers and the core structure of cellulose was intact as it contained carbon, oxygen and hydrogen. Further no nitrogen was present in the heated fibers which may be due to absence of proteins. Proteins are completely removed during soda cooking process due to their solubility in alkali. It was also observed that the content of carbon decreased whereas the content of oxygen increased indicating large structural differences. The O/C ratio for is 0.83 for cellulose which is in the typical range of cellulose (0.83) indicating that the samples consisting of only carbon and hydrogen are mainly carbohydrates i.e. showing absence of nitrogen.

Characterization of Synthesized polyol based Polyurethane with varying Hard to Soft Segment Ratio

In the preceding section the focus was on the isolation of CNFs and optimization of lignin extraction from waste jute bags using soda cooking process and further modification of extracted soda lignin to lignopolyol by oxypropylation mechanism. Various physicochemical, morphological and compositional characteristics of cellulose nanofibrils, lignin and lignopolyol were discussed.

In this section the focus is on the study of numerous properties of the lignopolyol based polyurethane synthesized using solvent evaporation method resulting from reaction of PO, BDO and MDI with varying hard to soft segment ratio. The methodology has been explained in section 2.2.6. Various analytical techniques like FTIR, XRD, TGA, DSC and tensile testing were used for the study of structure, morphological, thermal and mechanical properties of synthesized polyurethane. Also the ratios of hard to soft segment were optimized to obtain best thermal and mechanical properties. Polyurethane samples with varying hard to soft segment ratios are indicated as PU1, PU2, PU3 and PU4; their detailed nomenclature has been indicated in table 2.3, 2.2.6.

FTIR Analysis

FTIR spectra of Lignopolyol, MDI and lignopolyol based polyurethanes with varying hard to soft segment ratio is shown in figure 17 (i) and 17 (ii), respectively. Also, the observed prominent peaks with their band descriptions are tabulated in table 6.

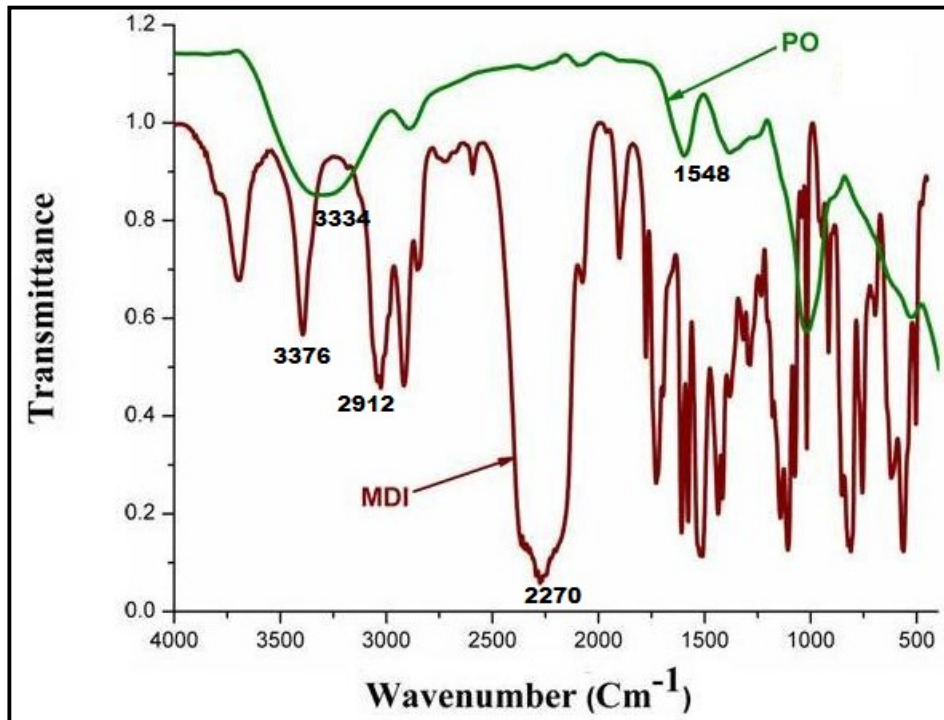


Figure 17 (i): FTIR spectra of Lignopolyol and MDI

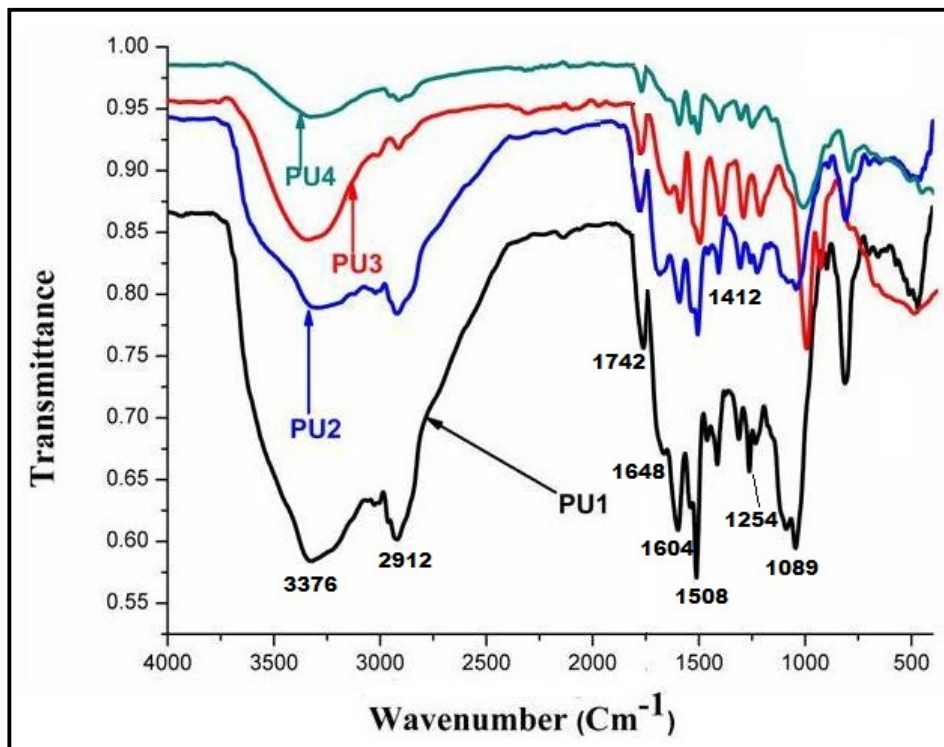


Figure 17(ii): FTIR spectra lignopolyol based polyurethanes with varying hard to soft segment ratio

Table 6: Prominent peaks with their corresponding band description of lignopolyol based polyurethanes with varying hard to soft segment ratios

Observed Peaks	Bands/Peaks Description
3334-3376	Hydrogen-bonded N-H stretching vibration [416]
2912-2914	C–O–C stretching vibrations [417]
1742	-NHCOO stretching combined with ester -COO stretching [417].
1648	Hydrogen bonded carbonyl group of urethane linkage [418,419]
1604	–C=C stretching due to aromatic ring of MDI [417]
1508	
1410-1413	C–O–C bending vibrations [417]
1304-1312	C–O–C wagging vibrations [417]
1254	–C–O–C stretching vibration in hard and soft segments [417]
1089	C–O–C stretching vibration of ether group [417]

Broad Hydroxyl peaks are observed in the spectra of lignopolyol and MDI due to the presence of moisture seen at 3454, 3100 and 3450 cm^{-1} , respectively. A characteristic peak of isocyanate is seen at 2270 cm^{-1} in the spectra of MDI. A narrow peak for carbonyl group is observed at 1548 cm^{-1} in FTIR spectra of lignopolyol.

Important feature of PU polymer is hydrogen bonding between urethane linkages that has a significant effect on its properties. Polyurethanes include different hydrogen bonds such as N-H bonds of the amide group as the donor and the urethane carbonyl, the ether oxygen, or the carbonyl group in the lignopolyol as the acceptor. Single stretching band at $\sim 3334\text{-}3376 \text{ cm}^{-1}$, corresponds to the hydrogen-bonded N-H stretching vibrations. Absence of peak between 3400 - 3500 cm^{-1} indicate that the all amide groups present in polyurethane films are involved in hydrogen bonding. Peak due to urethane carbonyl group (C=O) and ester groups i.e. NHCOO stretching combined with ester -COO stretching is seen around 1742 cm^{-1} . Peak near 1648 cm^{-1} represents ordered/crystalline region hydrogen bonded carbonyl in urethane groups that can be

seen in all the spectra but for PU2 this peaks is broadest which may be due to higher hard segment content.

Further, it was also observed that the intensity ratio of peaks corresponding to the hydrogen-bonded and the non-hydrogen-bonded carbonyl groups increases with increase in BDO content suggesting increased intermolecular interaction of hard and soft segment. This may be attributed to increased OH functionality resulting in the higher crosslinking and an increased urethane content. Bands at $2912\text{--}2914\text{ cm}^{-1}$, $1410\text{--}1413\text{ cm}^{-1}$ and $1304\text{--}1312\text{ cm}^{-1}$, respectively, are attributed to stretching, bending and wagging vibrations of $-\text{CH}_2$ group, along with bands at 1508 cm^{-1} and 1604 cm^{-1} due to $-\text{C}=\text{C}$ stretching in aromatic ring of MDI. Peaks at 1089 cm^{-1} is due to the ether group $\text{C}-\text{O}-\text{C}$ stretching vibration. A very strong band at 1254 cm^{-1} is assigned to $-\text{C}-\text{O}-\text{C}$ stretching vibration in hard and soft segments. Disappearance of peak around 2270 cm^{-1} signifies the complete curing and reaction of soft and hard segment with the successful synthesis of PU. Also, $\text{C}-\text{O}-\text{C}$ stretching absorption band corresponding to the chemical linkage between OH and NCO groups to form urethane bond also provide strong evidence for the formation of PU.

3.4.2 XRD Analysis

X-ray diffraction patterns of the lignopolyol based polyurethane (LPU) with varying soft to hard segment ratios are shown in Figure 18. From the figure, it is observed that the XRD diffractograms exhibits broad peaks at 2θ angles around 9° , 12.5° , 20° and 26.8° , respectively indicating moderate degree of crystallinity. Effect of variation in PO and BDO concentrations on degree of crystallinity was studied as it relates to the interaction of hydrogen bonding between the soft and hard segment. Further, from the figure, it was observed that the LPU with same molar concentration of PO and BDO i.e. 1:1 and 0.45:0.55 shows the maximum crystallinity as evidenced from high intensity peaks at 2θ angles, 20° and 26.8° , which may be due to trifunctional active sites that increases the degree of crystallinity. With the change in the molar ratio of PO and BDO to 0.25:0.75 and 0.75:0.25, respectively, peaks located at 2θ angles 20° and 26.8° become broader showing a decrease of crystallinity in the sample. From these results it can be concluded that the crystallinity is controlled by the variation in hard and soft segment which may be attributed to the degree of cross linking of polyurethane controlled by the hydroxyl group existing in the lignopolyol. Thus, increasing the molar ratio of lignopolyol to butanediol decreases the urethane cross linking.

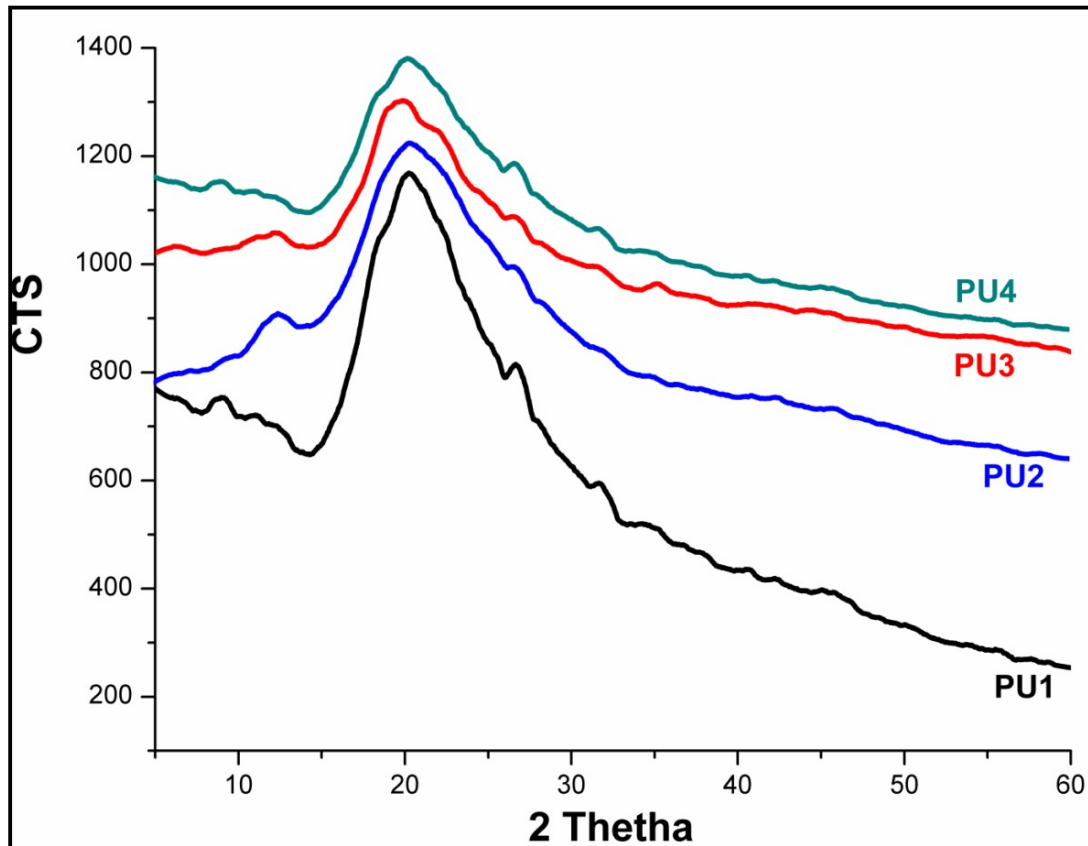


Figure 18: XRD of lignopolyol based polyurethanes with varying hard to soft segment ratio

TGA Analysis

TGA determines the amount of weight loss of a material as a function of temperature or time in a controlled atmosphere. As materials are heated, they can lose weight by simple processes such as drying, oxidation and chemical changes that liberate gases and lighter fragments. Some materials can gain weight by reacting with the atmosphere in the testing environment. Since weight loss and gain completely destroy the material, knowledge of the magnitude and temperature range of related reactions are necessary in order to design adequate thermal ramps and holds during those critical reaction periods. The technique is best suited to characterize the materials that exhibit weight loss or gain due to decomposition, oxidation, or dehydration. The first derivative (DTG) of TGA indicates the corresponding rate of weight loss. The peak of DTG curves i.e. DTG_{max} gives the highest rate of thermal decomposition and can be used as a means to compare thermal stability characteristics of different materials.

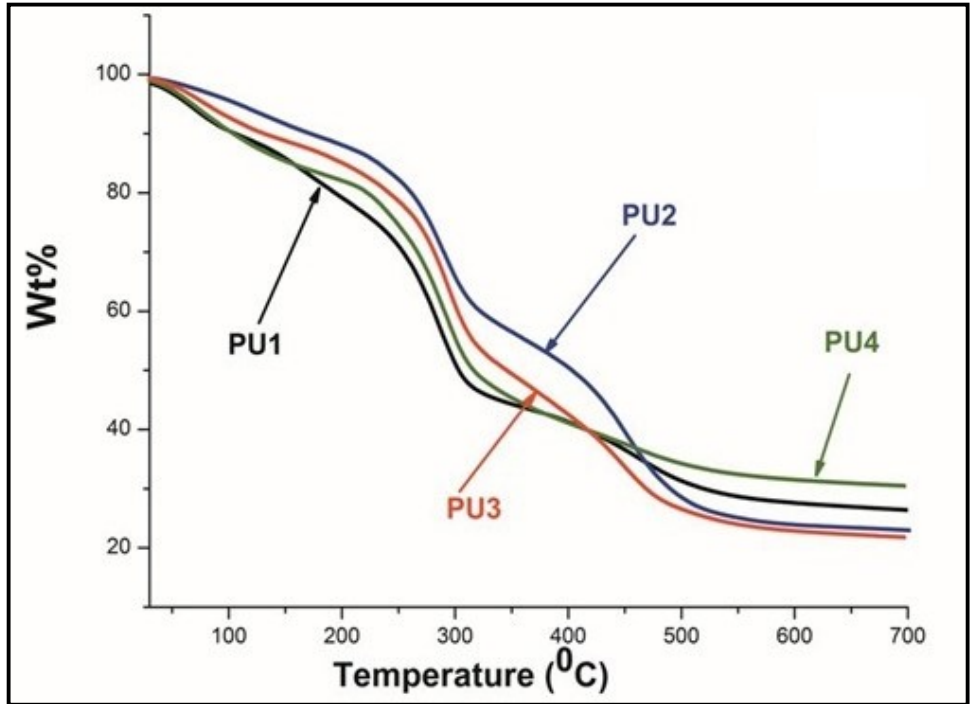


Figure 19 (i): TGA curves of lignopolyol based polyurethanes with varying hard to soft segment ratio

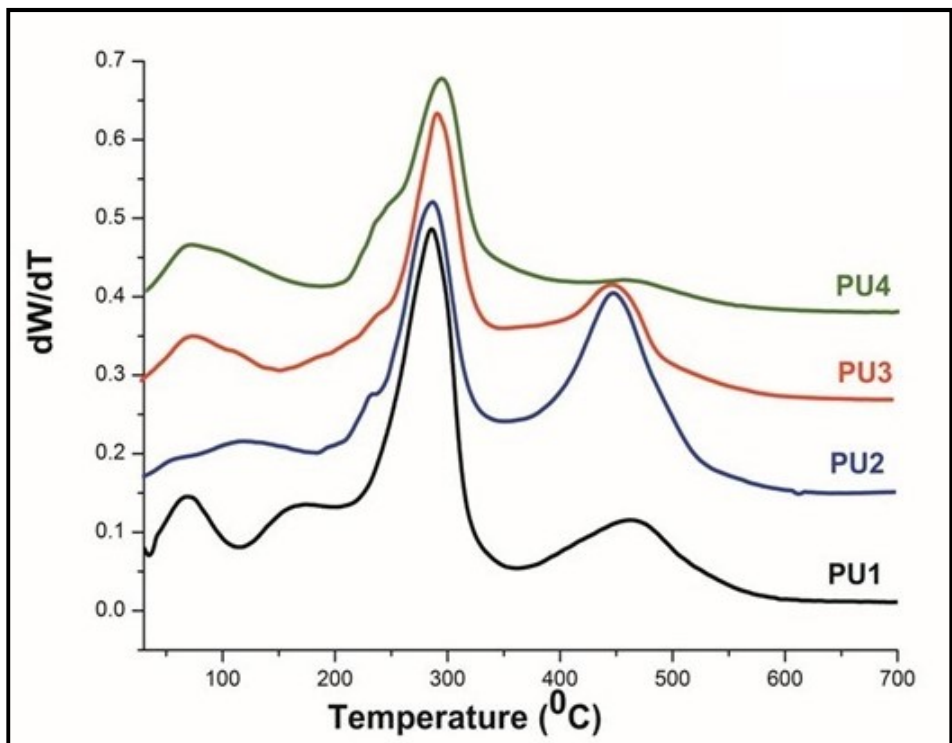


Figure 19 (ii): DTGA curves of lignopolyol based polyurethanes with varying hard to soft segment ratio

Figure 19 (i) and figure 19 (ii), respectively shows the TGA and DTG curves of LPU synthesized with different hard to soft segment ratios. Also the percent mass loss at different degradation temperatures, DTG_{max} and T_{onset} are summarized in table 3.17. From the figure, it was observed that the polyurethane degradation takes place in three steps. The first degradation below 100 °C may be due to traces of moisture in the LPU films while the second degradation observed between 200 to 300 °C corresponds to urethane bond decomposition either due to isocyanate and polyol dissociation or the due to the amines or olefins formation. The third degradation that takes place from 400-500 °C may be due to lignopolyol scission and hence in case of PU3 the % mass loss in this region is maximum.

Hence, three step degradation was observed for all LPU films; in the first step degradation is due to moisture in the all LPU films, while in the second step urethane degradation temperature and % mass loss for PU1 and PU4 was higher than the PU2 and PU3 and maximum for PU1 which may be due the same composition of the hard and soft segment resulting in higher degree of crosslinking, crystallinity and hydrogen bonding interaction that was also confirmed by FTIR and XRD results, while in the second step, % mass loss was less for PU1 and PU4 which may be due to presence of large quantity of free hydroxyl groups.

Table 7: Thermal decomposition characteristics of lignopolyol based polyurethanes with varying hard to soft segment ratios

1 st Thermal event				2 nd Thermal event			
Sample ID	T_{onset} (°C)	T_{max} (°C)	%Mass loss at T_{max}	T_{onset} (°C)	T_{max} (°C)	%Mass loss at T_{max}	% Mass Residue at 700 °C
PU1	260	300	41.42	422	462	10.50	27.50
PU2	240	286	33.29	420	444	32.30	19.71
PU3	246	288	32.30	425	445	31.51	18.55
PU4	256	298	40.30	419	460	16.60	22.98

The overall thermal degradation was determined from TGA curves using onset degradation method. From the data in table 1 it can be seen that for LPU films with varying hard to soft segment ratio, the T_{max} for urethane bonds decreases from 300 to 286 °C with decrease in molar ratio of lignopolyol and BDO from 1 to 0.75 and 0.25. This may be attributed to the decreased crystallinity as it controls the crosslinking of urethane groups. Also from the table it was observed that onset thermal degradation temperature i.e. T_{onset} increases with increase in hard segment and is maximum for the sample PU1. Similar trends were seen for percent mass residue at 700°C. The percent mass residue increase from 18.55 to 27.50 for PU3 to PU1 thereby suggesting that the PU1 is thermally most stable out of all the samples. Also, the thermal stability of lignopolyol based polyurethane was found to be similar or higher than the commercially available polyurethanes such as polyethylene glycol, polypropylene glycol, castor oil and vegetable oil based polyurethanes.

Tensile Testing

Tensile measurements give important information regarding tensile strength, Young's modulus, %elongation and toughness of a material. The important structural parameters that control tensile strength and Young's modulus of segmented polyurethane are degree of crystallinity, crosslinking and intermolecular interaction. The tensile strength, Young's modulus and % elongation of lignopolyol based polyurethanes with varying hard to soft segments ratios were obtained from the stress strain curve (figure 20(a)) and are tabulated in table 8.

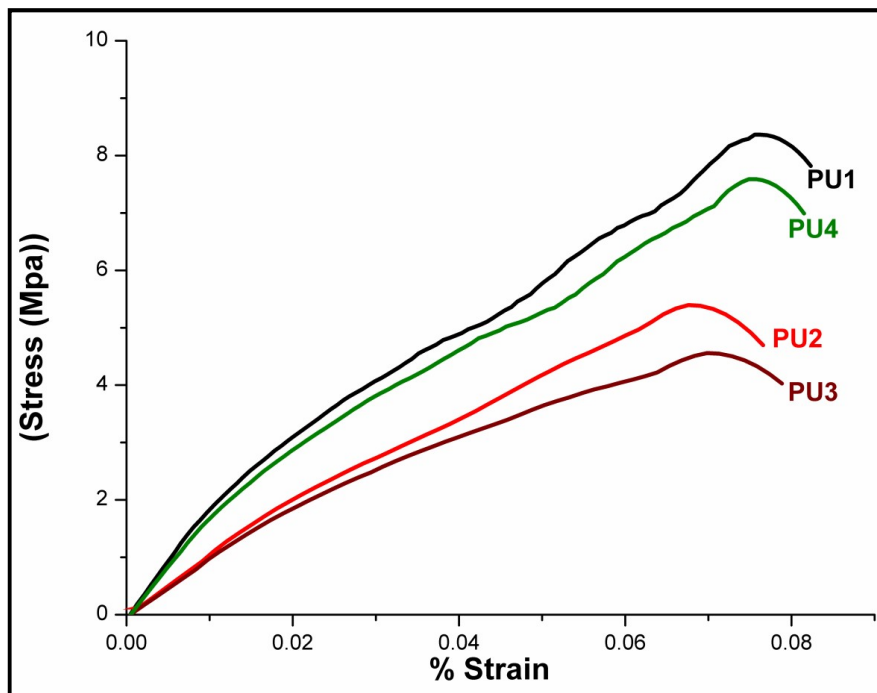


Figure 20 (i): Stress vs. Strain curves of lignopolyol based polyurethanes with varying hard to soft segment ratios

Table 8: Mechanical properties of polyurethanes with varying hard to soft segment ratios

Sample	Tensile Strength(MPa)	% Elongation	Young's Modulus (MPa)
PU1	8.4 ± 0.4	144 ± 4.3	247.06 ± 8.7
PU2	5.1 ± 0.3	320 ± 14.2	175.86 ± 5.3
PU3	4.7 ± 0.5	288 ± 9.2	142.42 ± 4.5
PU4	7.7 ± 0.4	192 ± 6.8	220.00 ± 6.4

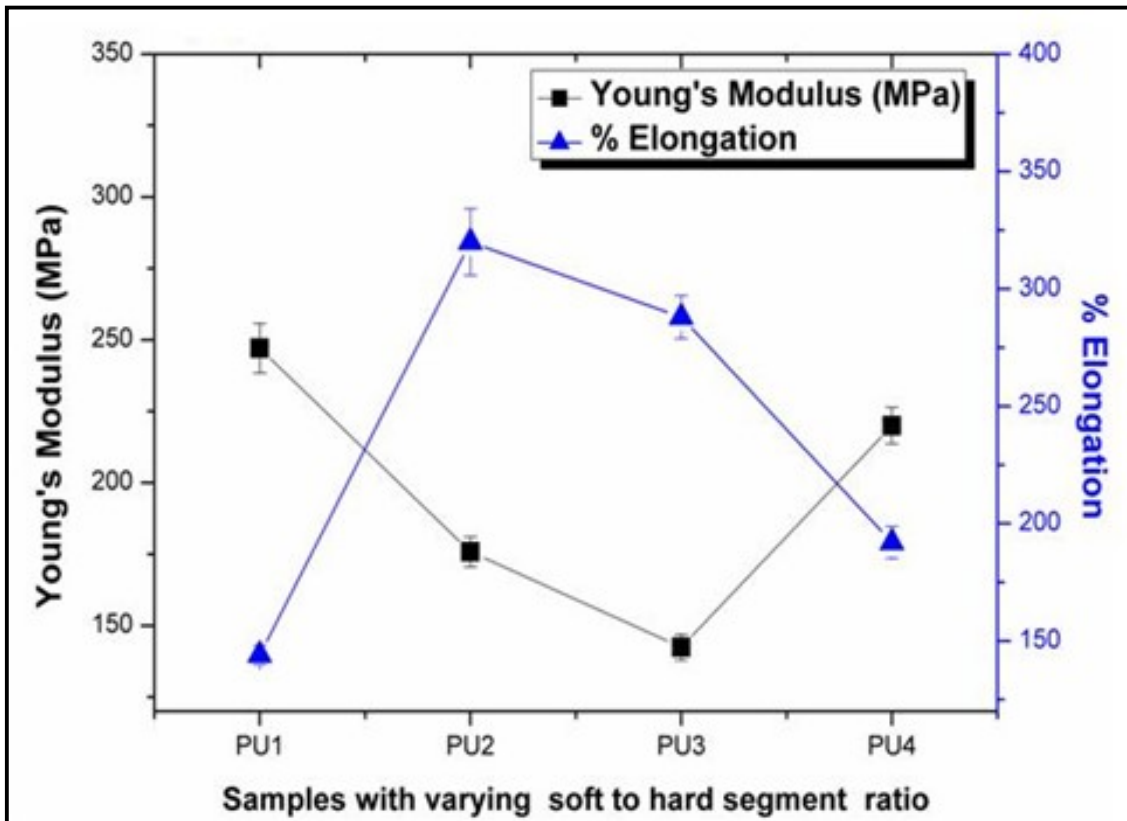


Figure 20 (ii): Young's modulus and % elongation of lignopolyol based polyurethanes with varying hard to soft segment ratios

From the results, it was observed that tensile strength and Young's modulus increases from 4.7 to 8.4 MPa and 142.42 to 247.06 MPa, respectively, with increase in hard segment content. It was maximum for the sample with equal composition of the hard and soft segment. The increase in Young's modulus and tensile strength may be attributed to increase in intermolecular bonding, degree of interconnectivity of hard and soft segment and degree of crystallinity of hard domains with the increase in concentration of hard segment as also confirmed by results of FTIR and XRD.

Further, the effect of filler content on percent elongation is shown in figure 20 (ii). It exhibits that increase in hard segment content results in decrease in % elongation and increase in Young's modulus i.e. polyurethanes with higher soft segment have elastomeric behavior whereas those with higher hard segment show an opposite trend which could be either because of soft segment potential to crystallize under strain or due to possibility of higher crystalline region formation with higher hard segment content. These results are in coherence with that reported in

literature. Further Young's modulus and tensile strength of lignopolyol based polyurethanes was found to be comparable with polyurethane synthesized using other polyols[429–432]. Hence, these polyurethanes were further used for synthesizing nanocomposites with varying amount of CNFs.

Characterization of Synthesized Lignopolyol Based Polyurethane/Cellulose Nanofibers (PU/CNF) Nanocomposites

Lignopolyol/cellulose nanofibrils based polyurethane nanocomposites with varying weight percentage of CNF i.e. 2.5, 5, 10 & 15% were synthesized by incorporating them to lignopolyol based polyurethanes with equal amount of hard and soft segment i.e. PU1 using solvent evaporation method. Prepared nanocomposites were characterized for structural and morphological characteristics using FTIR, WD-XRD and SEM. Further, the effect of reinforcement on enhancement of thermal and mechanical properties was evaluated using TGA, DSC and tensile testing, respectively. Lignopolyol based polyurethane/cellulose nanofibers (PU/CNF) nanocomposites with varying weight percentage of cellulose nanofibrils are designated as PU, NPU1, NPU2, NPU3 and NPU4, respectively.

3.5.1 FTIR Analysis

Fourier transform infrared spectroscopy is used to analyze the chemical structure of polyurethane and its nanocomposites. FTIR spectra and various prominent peaks of lignopolyol based polyurethane and its nanocomposites are shown in Figure 21 and table 9, respectively. A broad band at 3320-3324 cm^{-1} can be related to the hydrogen bonded -NH stretching vibrations of urethane linkage or due to O-H stretching vibration of cellulose seen in all the spectra except for NPU4 which may be due to agglomeration of fibers at higher concentration resulting in the decreased interaction of hard and soft segment.

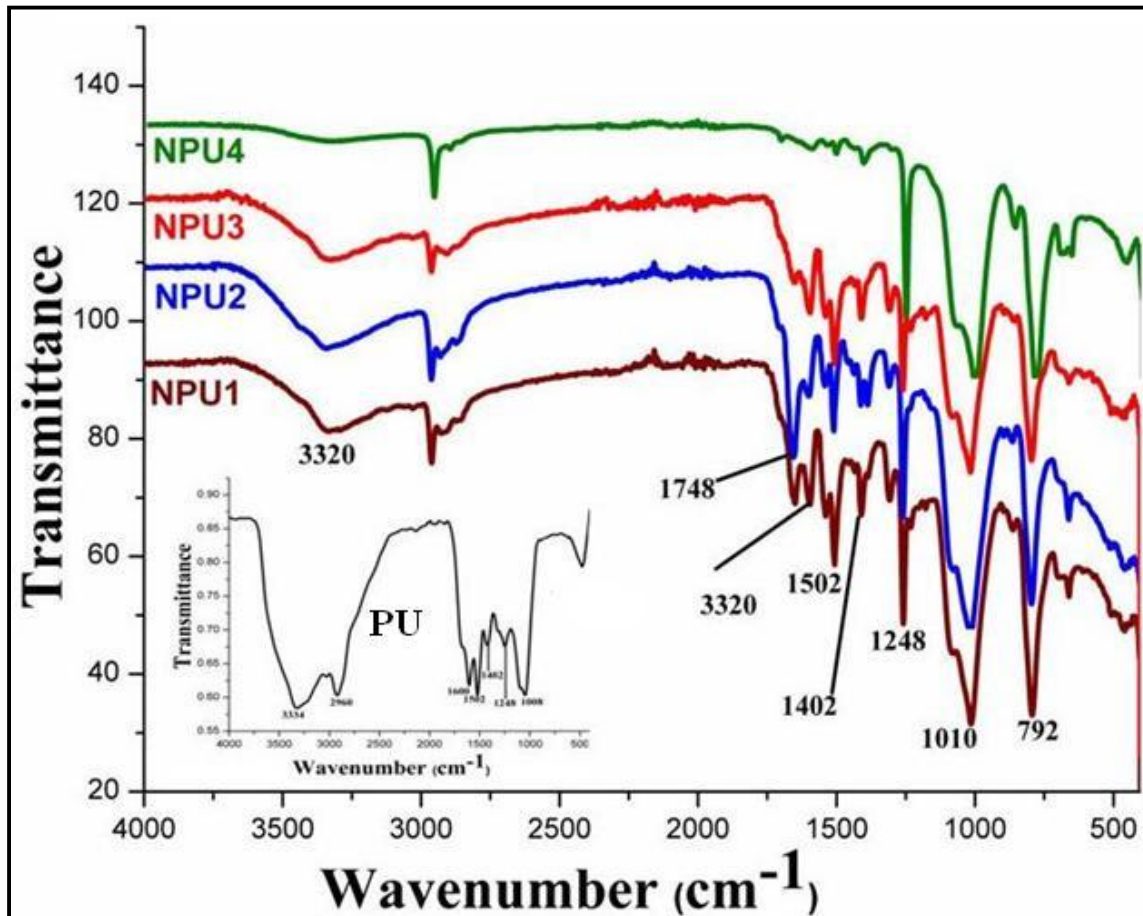


Figure 21: FTIR spectra's of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

The peak at $2960\text{-}2970\text{ cm}^{-1}$ is due to asymmetric stretching vibrations of $-\text{CH}_2$. Peaks at $1734\text{-}1748\text{ cm}^{-1}$ correspond to urethane and ester stretching vibrations that corroborate the infusion of hard and soft segment in polyurethane matrix. Further as the filler concentration increase from 2.5 to 15% the carbonyl stretching peaks are displaced from 1734 to 1748 cm^{-1} suggesting that the reinforcement of CNF in PU matrix resulted in distortion of NH and C=O hydrogen bonding and improved micro phase separation between hard and soft segments because of increased interaction of CNF and PU matrix. Peaks between $1600\text{-}1648\text{ cm}^{-1}$ and $1502\text{-}1510\text{ cm}^{-1}$ are due to C=O stretching vibration of urea and C-N stretching or N-H out of plane bending.

The peak at $1402\text{-}1404\text{ cm}^{-1}$ seen only in case of PU/CNF nanocomposites correspond to skewing of C-H bond thereby exhibiting the crystalline behavior of reinforced cellulose nanofibers. Bands at $1248\text{-}1252\text{ cm}^{-1}$ and $1008\text{-}1010\text{ cm}^{-1}$ relate to the stretching vibration of C-

N and C-O, respectively thereby affirming the formation of urethane linkages between lignopolyol hydroxyl and NCO group of isocyanates. Further, the disappearance of isocyanate peak at 2270 cm^{-1} confirmed the completion of reaction. The PU/CNF nanocomposites showed similar peaks but with the varying intensities. The intensity of the peak at 3320 cm^{-1} due to cellulose O-H stretching vibrations and N-H stretching vibrations decreases with increase in filler concentration and almost disappeared for nanocomposites with 15% CNF concentration that may be due to hydroxyl groups on cellulose reacting with isocyanate during PU synthesis. Overall, it was observed from the FTIR spectra that CNF reinforcement does not affect the structure and hydrogen bonding between NH and C=O of polyurethane till 10% CNF concentration beyond which the intensity of urethane linkage starts decreasing.

Table 9: Prominent peaks with their corresponding band description of lignopolyol based polyurethane/cellulose nanofibers (PU/CNF) nanocomposites

Observed Peaks/Bands	Bands Descriptions
3320-3324	-NH stretching vibrations of Urethane or O-H stretching vibration of cellulose [438,439]
2960-2970	Asymmetric $-\text{CH}_2$ stretching vibrations [440]
1734-1748	Urethane and ester stretching vibrations [441]
1600-1648	C=O urea stretching [443]
1502-1510	C-N stretching or N-H out of plane bending [443]
1402 -1404	C-H bond deformation [441]
1248-1252	Stretching vibration of C-N [438]
1008-1010	C-O stretching vibration [439]

XRD Analysis

X-ray diffraction technique was used to get information regarding crystalline behavior of PU/CNF nanocomposites films. Figure 22 shows the XRD patterns of cellulose nanofibers and lignopolyol based polyurethane nanocomposites. From the figure, it was observed that cellulose nanofibers show three peaks at 12.5° , 20.5° and 22.6° 2θ angle, respectively. Where peak at 12.5° and 20.5° 2θ angles correspond to cellulose II, peak at 22.6° 2θ angle corresponds to native cellulose I revealing the coalescence of cellulose I and II that has already been explained. For lignopolyol/cellulose nanofibers based polyurethane nanocomposites only a broad hump was observed between 20 - 23° 2θ till 10% CNF concentration beyond which a single peak at 22.6° 2θ angle was seen, confirming that the cellulose nanofibers were well dispersed in PU matrix up to 10% filler concentration. This may be due to the strong interaction between carbonyl group of PU matrix and hydroxyl group of CNF originating from hydrogen bonding. But beyond 10% filler concentration CNFs started agglomerating as also confirmed from SEM results. This agglomeration may be either due to the high surface energy of cellulose or due to the hydrophilic character of the cellulose that causes the irreversible agglomeration because of the formation of additional hydrogen bonds between the amorphous parts of the CNFs.

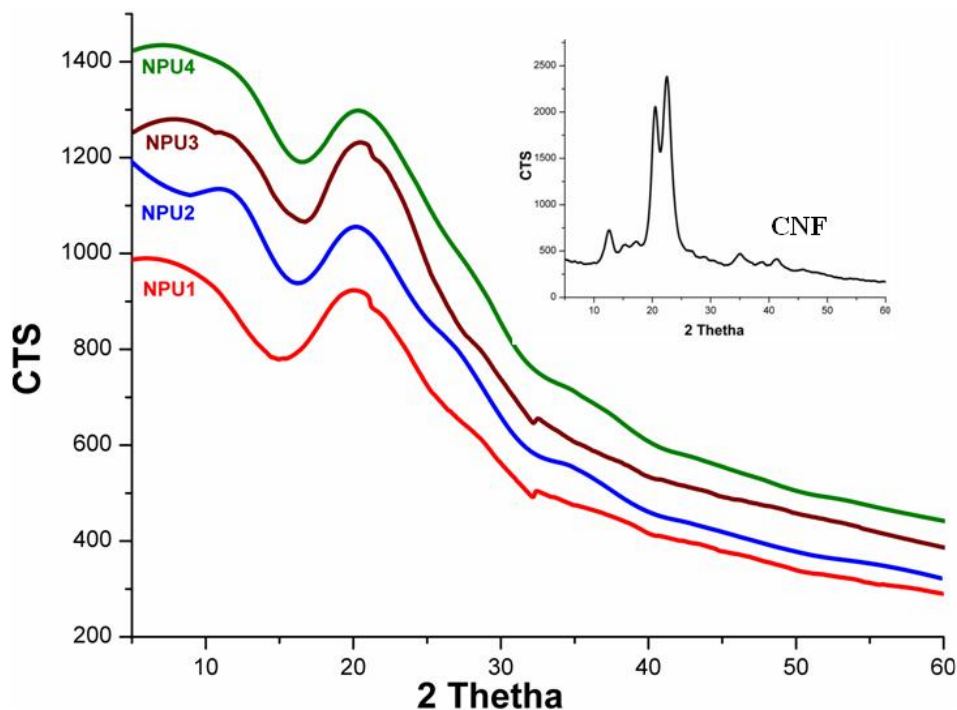


Figure 22: X-ray diffractograms of lignopolyol based polyurethane and its nanocomposite with varying filler concentration

SEM Analysis

The various properties of polyurethane nanocomposites not only depend on the interactions between soft and hard segments or the interaction of PU matrix with fillers but also on the micro phase structure and level of dispersion of nanofibers that can be well studied by SEM analysis. SEM images of CNF, neat PU and (PU/CNF) nanocomposites with varying filler concentrations are shown in figure 23. From SEM images of PU/CNF nanocomposites (figure 23 (c-f)), it was observed that CNFs are homogeneously dispersed in polyurethane matrix. PU is visible as amorphous phase in the background and CNFs are seen as fibers. The structure is intact and there is a good adhesion between PU and CNF as seen in SEM images.

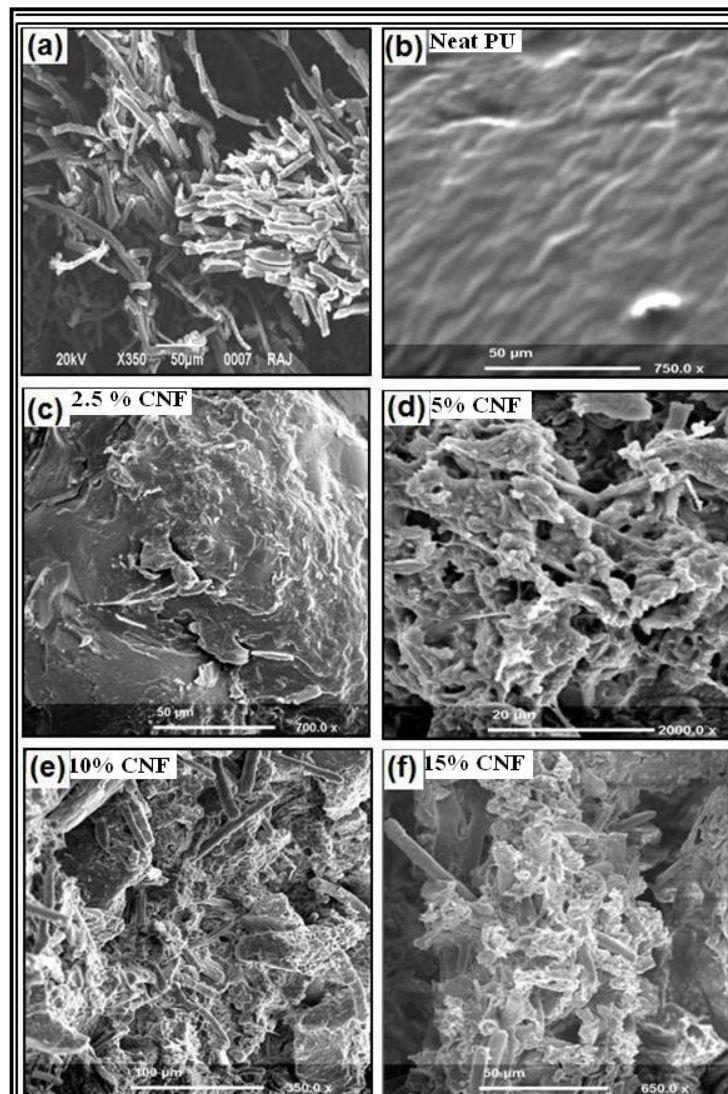


Figure 23: SEM micrographs of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

It was also observed that the structure of fractured PU/CNF nanocomposites with 2.5 wt% (figure 25 (c)) filler concentration was not much affected with the incorporation of cellulose nanofibers and only small white dots were seen on the overall surface. This is due to the fact that at lower filler concentration cellulose nanofibers are uniformly dispersed in the polyurethane matrix because of the strong hydrogen bonding that results in good adhesion of CNF with PU matrix. However, fibers bundles were observed for PU/CNF nanocomposites with 5, 10 and 15% filler concentration. Moreover, cellulose nanofibers were uniformly dispersed throughout the surface of polyurethane matrix up to 10% filler concentration beyond which complete agglomerated fibers were seen. This agglomeration may be attributed to the weak interaction of polymer matrix and cellulose nanofibers at higher filler loading. These results are in coherence with XRD results.

Overall, from SEM results, it was concluded that the morphology of PU/CNF nanocomposites was influenced by crystalline structure of cellulose nanofibers and presence of surface hydroxyl groups that has lead an excellent interaction between CNF and polymer matrix. This homogenous dispersion and good interaction results in enhanced physical, thermal and mechanical properties of the nanocomposites.

Tensile Testing Analysis

The mechanical properties of the neat PU and PU nanocomposite films were measured under tensile stress at room temperature. Stress vs. Strain curve of neat and polyurethane nanocomposites with varying filler content is shown in figure 24 (i). Tensile strength, Young's modulus and % elongations obtained from tensile measurements are summarized in table 10. Also the variation in Young's modulus and % elongation with varying filler concentration is shown in figure 24(ii). From these results it was observed that the cellulose nanofibers have profound effect on the mechanical properties of polyurethane nanocomposites. From the results, it is clearly seen that the tensile strength and Young's modulus increases while the percent elongation decreases with incorporation of cellulose nanofibers into PU matrix. The increase in tensile properties may be attributed to the formation of new interconnected cellulosic network facilitated by their flexibility due to high aspect ratio and the presence of amorphous domain along the nanofibrils. Nevertheless, other important parameters that explain the better mechanical properties of CNF based nanocomposites are network structure of lignopolyol

structure and high tensile strength (0.3-22 GPa) of cellulose nanofibers. However, it was observed that tensile properties of CNF reinforced polyurethane nanocomposites showed an improvement up to 10% filler concentration beyond which a slight decrease was observed. This decrease in tensile properties may attributed to aggregation of the nanofibers, driven by their high affinity for each other [457]. As, the agglomeration may result in commencement and proliferation of cracks thereby reducing the strength of nanocomposites. The factors important for enhanced tensile strength and Young's modulus are aspect ratio, fiber interaction between filler and polymer matrix and dispersion of filler. The mechanical properties of PU/CNF were found to be comparable with nanocomposite synthesized using other fibers such as kenaf fibers.

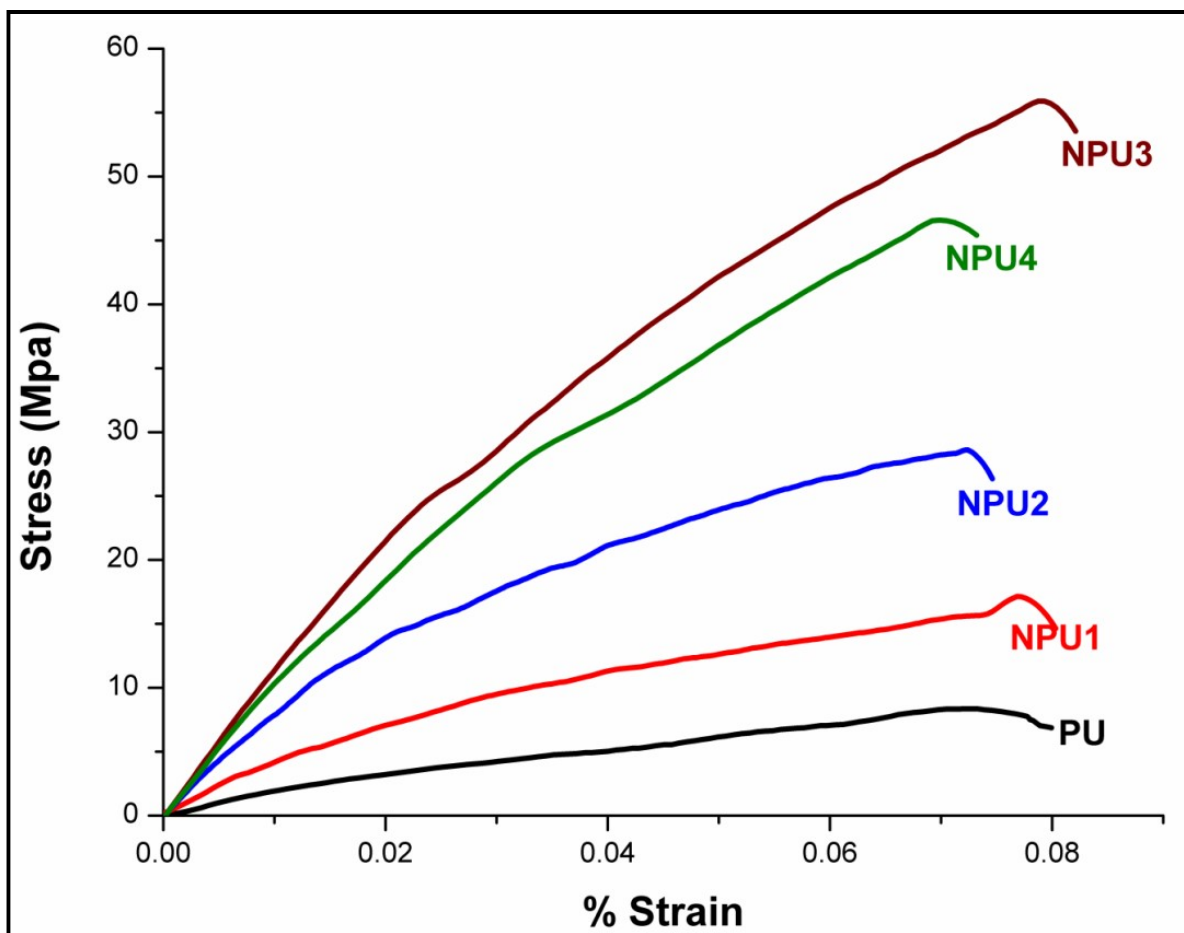


Figure 24(i): Stress vs. Strain curve of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

Table 10: Tensile Strength, % elongation and Young's modulus of lignopolyol based polyurethane/cellulose nanofibers (PU/CNF) nanocomposites

Sample	Tensile Strength(MPa)	% Elongation	Young's Modulus (MPa)
PU1	8.4± 0.4	144±4.2	247.06±8.7
NPU1	16.5± 0.3	136±6.8	402.44±18.2
NPU2	27.9± 0.5	123.2±9.2	429.23±20.6
NPU3	54.5± 0.4	97.6±14.2	801.47±21.8
NPU4	46.8± 0.3	110.4±16.6	557.14±23.2

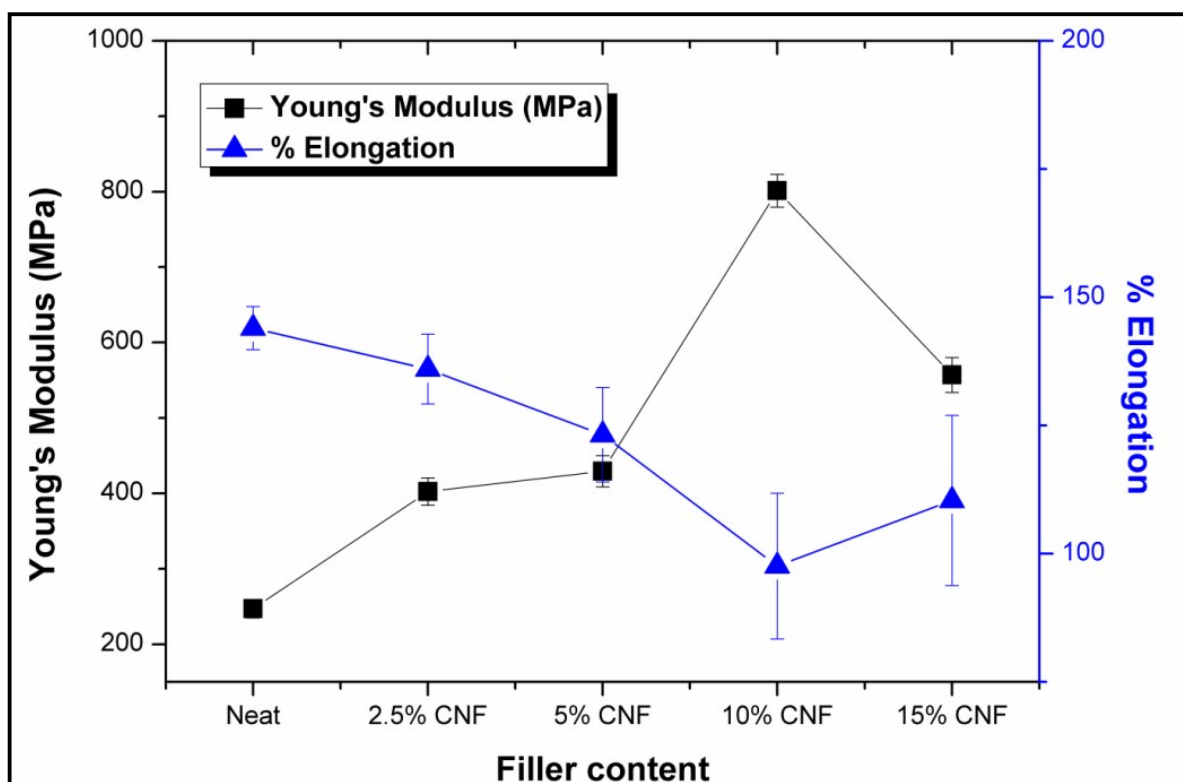


Figure 24(ii): Young's modulus and % elongation vs. filler content of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

TGA Analysis

Thermogravimetric analysis (TGA) is a powerful technique for the measurement of thermal stability of materials including polymers. In this method, changes in the weight of a specimen are measured while its temperature is increased. Moisture and volatile contents of a sample can be measured by TGA. Thermo gravimetric analysis (TGA) was performed on the neat and cellulose nanofibers reinforced lignopolyol based polyurethanes nanocomposites and the % mass loss due to valorization of the products was monitored.

Figure 25 (i) and 25 (ii) show the TGA and DTGA curves of lignopolyol/CNF based polyurethane nanocomposites films with varying filler concentration. The thermal degradation parameters such as T_{onset} , T_{max} , their corresponding mass loss and % mass residue at 700 °C are given in table 11.

From the figures, two stage thermal decomposition was observed for neat and CNF reinforced polyurethanes, where the first decomposition at a T_{max} of 282-300 °C corresponds to the urethane linkage and the second at a T_{max} of 460-500 °C may be either due to chain scission at the β -position to the carbon-carbon double bond of polyurethane matrix or may be due to the formation of new bonds by the reaction of MDI and hydroxyl groups of cellulose nanofibers.

From the results it was seen that for the 1st degradation stage, the T_{max} varies from 282-300 °C and T_{onset} temperature increases with increase in filler concentration up to 10% CNF, beyond which it decreases. The increase in thermal stability up to 10% that may be due to enhanced molecular interaction of polyurethane matrix with cellulose nanofibers because of the polar nature of both cellulose nanofibers and polyurethane matrix and also due to the strong hydrogen bonding of PU/CNF nanocomposites generated because of the hydroxyl groups of cellulose thereby resulting in uniform and homogeneous dispersion of cellulose nanofibers in polyurethane matrix as also evidenced from earlier results.

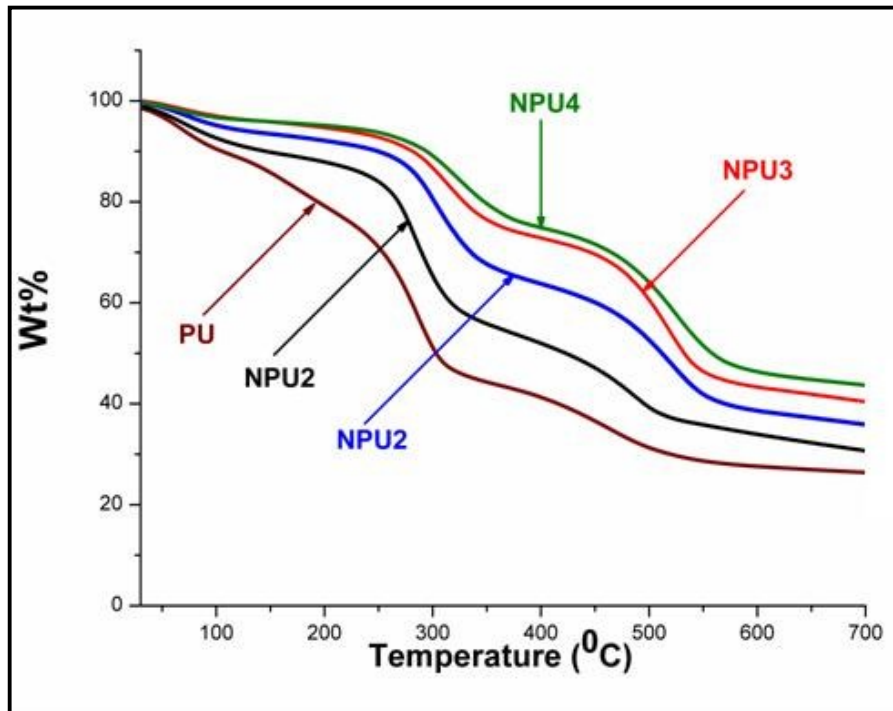


Figure 25(i): TGA curves of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

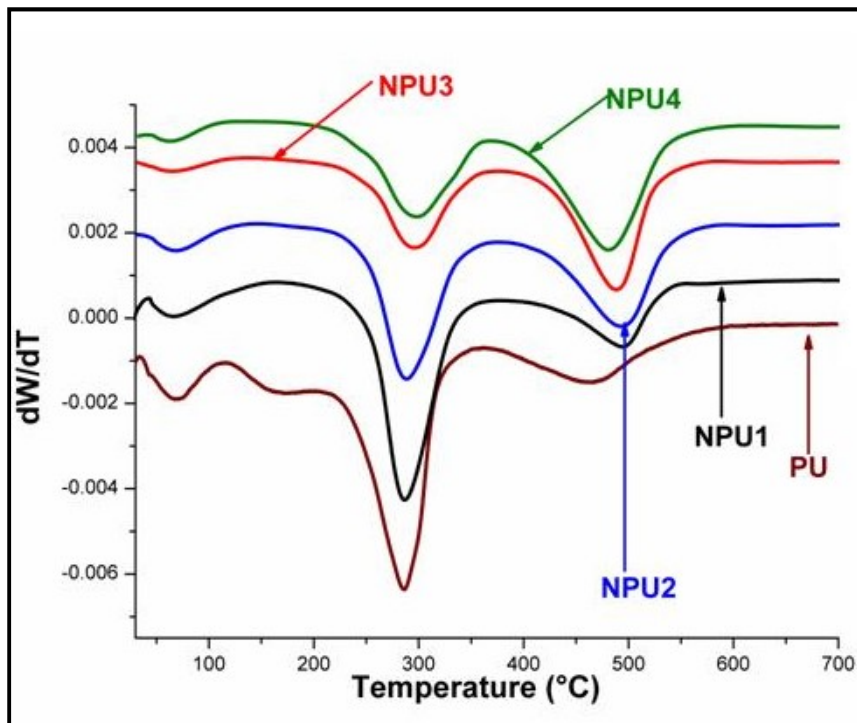


Figure 25(ii): DTGA curves of lignopolyol based polyurethane and its nanocomposites with varying filler concentration

Table 11: Thermal degradation characteristics of lignopolyol based polyurethane/cellulose nanofibers (PU/CNF) nanocomposites

Sample ID	1 st Thermal event			2 nd Thermal event			
	T _{onset} (°C)	T _{max} (°C)	%Mass loss at T _{max}	T _{onset} (°C)	T _{max} (°C)	%Mass loss at T _{max}	% Mass Residue at 700 °C
PU	220	282	40.96	380	460	66.52	27.50
NPU1	240	290	36.31	430	495	64.65	30.58
NPU2	248	296	24.40	440	500	58.24	34.95
NPU3	276	300	34.71	450	506	49.06	38.76
NPU4	262	294	19.92	438	483	53.31	44.81

The decrease in thermal stability beyond 10% may be attributed to aggregation of cellulose nanofibrils at higher filler loading. The same trend was observed for the 2nd degradation stage which may be due to increase of cellulose concentration that results in the formation of new bonds and increase in hydrogen bonding which enhances the thermal stability. Further, % mass residue at 700 °C also increased with increase in filler concentration indicating the higher thermal stability of PU/CNF nanocomposites as higher is the %mass residue higher is the thermal stability. Results are in coherence with those reported in the literature. Thermal stability of PU/CNF nanocomposites was found to either higher or similar as compared to PU nanocomposites with other nanofillers such as grapheme, carbon nanotubes and nanoclay.

Hydrolytic Degradation of Polyurethane Nanocomposites in Phosphate Buffer Saline (PBS) with pH =7.4

Biodegradable polymer nanocomposites are important class of materials for biomedical application. All biodegradable polymers contain hydrolysable bonds and hence primarily they are easily degraded by adopting the hydrolytic and enzymatic degradation mechanism. To a lesser extent, they can also be degraded by oxidation that leads to the crack formation and propagation. Some of the important parameters affecting the biodegradability of polymers

include type of chemical bond, polymer crystallinity, hydrophilicity, composition, pH value, molecular weight, morphology and glass transition temperature. Among these type of chemical bond and time dependent molecular weight are the two most commonly used parameters to determine the degradation rate as the type of chemical bond determines the rate of hydrolysis.

Depending on the application, the degradation behavior of polyurethane can be tailored by altering ratio of hard to soft segments. However, the soft segment contents are considered as the degradation rate controlling parameters as it leads to the formation of degradable chemical bonds. These chemical bonds along with fragments containing urethane and urea with acid terminal groups are degraded by the presence of acids or alkaline compounds. Further, degradation of urethane groups to free polyamines can occur depending on the type of diisocyanate used. Generally, the degradation of polyurethane takes place in several steps. Initially, the non-crystalline regions react with water molecules resulting in increase in chain mobility that reconstructs them into new and more defective crystals. Thereafter, the rate of degradation is increased due to the autocatalytic effect arising from the acidic nature of carboxyl/hydroxyl end groups. Finally, the complete hydrolysis occurs at the crystalline region.

Hydrolytic degradation of polyurethane started with the diffusion of water in the amorphous or semicrystalline regions that leads to the breakage of ester bonds. Mobility of polymer chains within the amorphous regions increased after chain scission. No appreciable reduction in the sample weight takes place indicating they could remain inside the polyurethane network structure as reported in the literature. Thereafter, an increase in weight loss was observed due to increase of -COOH/-OH end-groups which act as auto catalyst and accelerate the degradation process, resulting in shorter and more number of polymeric chains. Finally, the crystalline regions become susceptible to hydrolysis. Further, the incorporation of cellulose nanofibers also had a significant effect on the biodegradability as the reinforcement of cellulose nanofibers in polyurethane affects the microphase separation structure. In fact, the nanofiller consist of rigid domains that establish physical interactions with the polymer chains of the polyurethane by mean of their surface chains and entities. It was observed that with increase in % CNF loading, % weight loss increases. The amount of weight loss of polyurethane nanocomposite in phosphate buffer saline (pH \approx 7.4) in 1, 2, 4, 6 and 8 weeks was obtained as explained earlier section and is shown in figure 26.

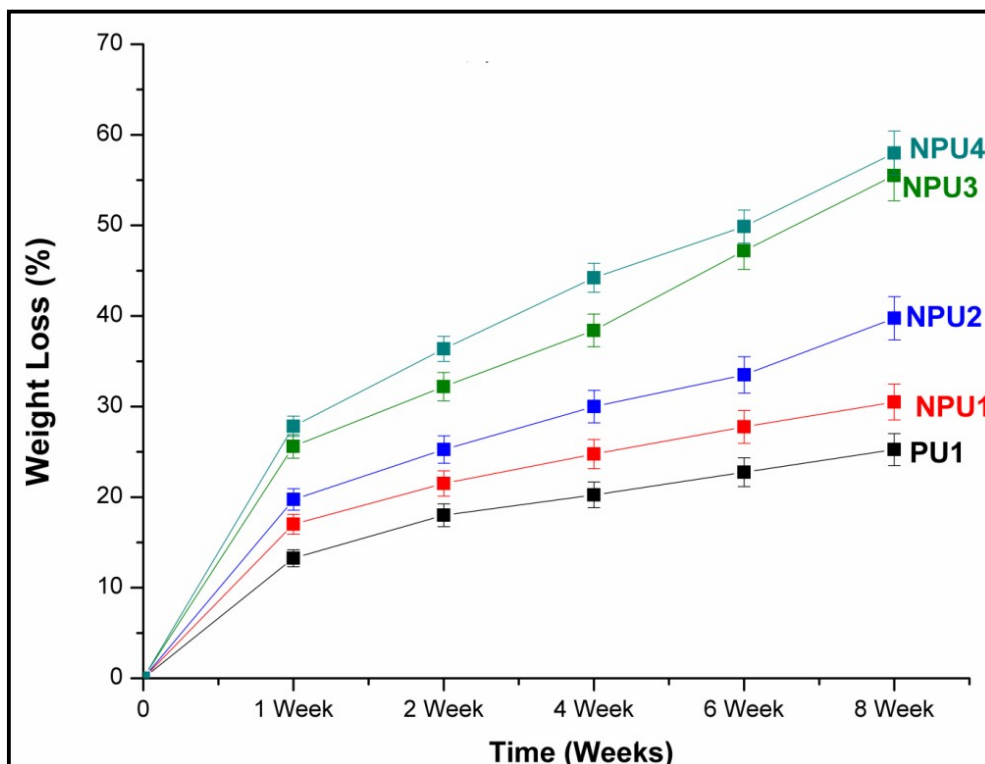


Figure 26: Percent Weight loss Vs. Time of lignopolyol based polyurethane nanocomposite with varying filler concentration from 0-15%

From the figure 3.26, it was observed that % weight loss after 8 weeks for neat polyurethane was 25.12%. With increase in filler content from 0 to 15% (w/w), % weight loss increased from 25.12 to 57.58%. This increase in weight loss may be attributed to the hydrophilic nature of cellulose nanofibers. Incorporation of hydrophilic component in polymer matrix can enhance water sorption and that might result in improved rate of hydrolysis of ester bonds present in polyurethane structure. Further, no decrease in the biodegradability was seen beyond 10% CNF concentration which may be also be due to the fact that with increasing amount of highly hydrophilic material in the nanocomposite film, possible infiltration of water molecules in the interfacial filler/matrix zone takes place. The higher the cellulose nanofiller content higher is the interfacial area and thus the possible interfacial water infiltration increases, which leads to higher chain scission rate and therefore, results in increase in % weight loss of polymer. Moreover, it was seen that the increase in percent weight loss was not much pronounced beyond 10% filler concentration thus PU nanocomposite with 10% CNF composition can be regarded as the suitable material for further applications. For this composition, the mechanical and thermal properties were also better than other nanocomposites.

Furthermore, the effects of degradation products on the pH value of the medium were also evaluated without refreshing the medium during the biodegradation period. It was observed that during the 8 weeks' degradation, value of pH decreased to 7.1 from 7.4. This decrease in pH value may be due to acidic groups released during the degradation of lignopolyol or 1, 4-butanediol.

Overall, it was concluded that hydrolytic degradation of lignopolyol based polyurethane is greatly influenced by the incorporation of cellulose nanofibers.

Antimicrobial Activities of Lignopolyol/CNF based Polyurethane Nanocomposites

Polymers and its nanocomposite being used for biomedical applications must possess antimicrobial activity and protection against biofilm formation by microorganism. *Staphylococcus aureus* (*S. Aureus*) and *Escherichia Coli* (*E.coli*) are among the most common pathogens and are related to many infections including wounds, postoperative infections and prosthetic infections taking place using the use of catheters, endotracheal tubes and other biomaterials.

In the present study the antimicrobial activity of lignopolyol based polyurethane nanocomposite films containing cellulose nanofibers as nanofiller was determined against Gram-positive *S. aureus* and Gram-negative *E. coli* microorganisms. It is well known fact that polyurethane inherently does not possess any antimicrobial activity and can be induced by addition of a compound with antimicrobial activities. Cellulose nanofibers with a three dimensional non-woven network an highly hydrophilic nature exhibits excellent physical and mechanical properties such as high water absorption capacity, tensile strength, good permeability, crystallinity and biocompatibility that make them suitable for various biomedical applications. Hence cellulose nanofibers can also be explored for antimicrobial activity. The antimicrobial activities of polyurethane nanocomposite studies as explained in section 2.8.14 and are shown in figure 27(i) and 27(ii). From the figures no change in the color of the suspension containing films was observed which shows that all the nanocomposites films were capable of inhibiting the growth of the colonies of *E. coli* and *S. aureus*. However, the nanocomposite films were found to be more effective in inhibiting the growth of *E. coli* than *S. aureus*. Further, it was also seen that with increase in % CNF loading in polyurethane, appreciable increase in antimicrobial activity towards *S. aureus* and *E. coli* which can be clearly seen from the images as the suspension containing film with 15% CNF loading was more clear. This increase in antimicrobial activity

may be attributed to the porous network structure of nanocellulose that promotes the transfer of antibiotics or other medicines serving as efficient physical barrier against any external infection [476].

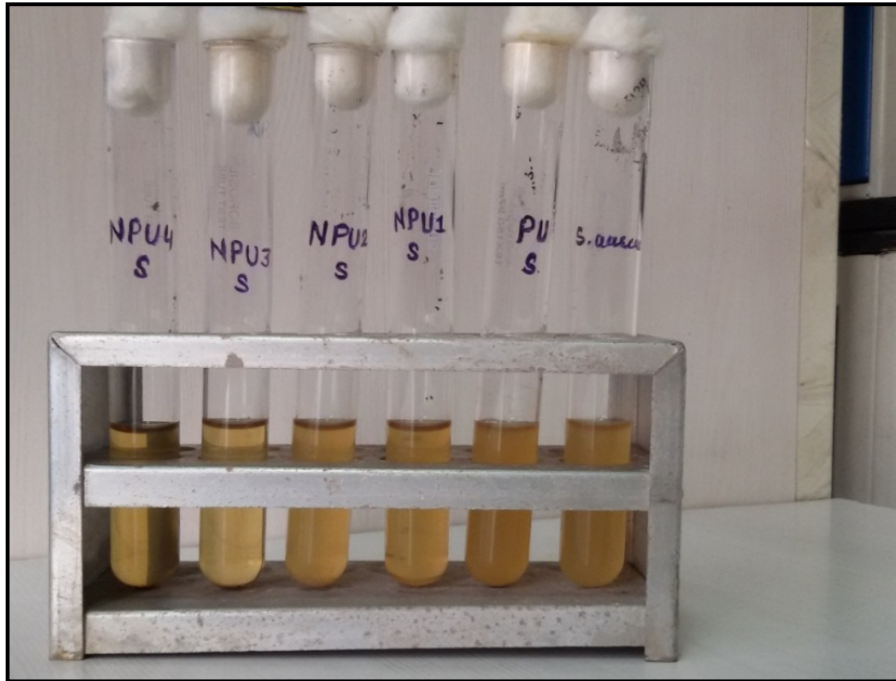


Figure 27 (i): Antimicrobial activity of lignopolyol based polyurethane nanocomposite with varying filler concentration from 0-15% against *S.aureus*

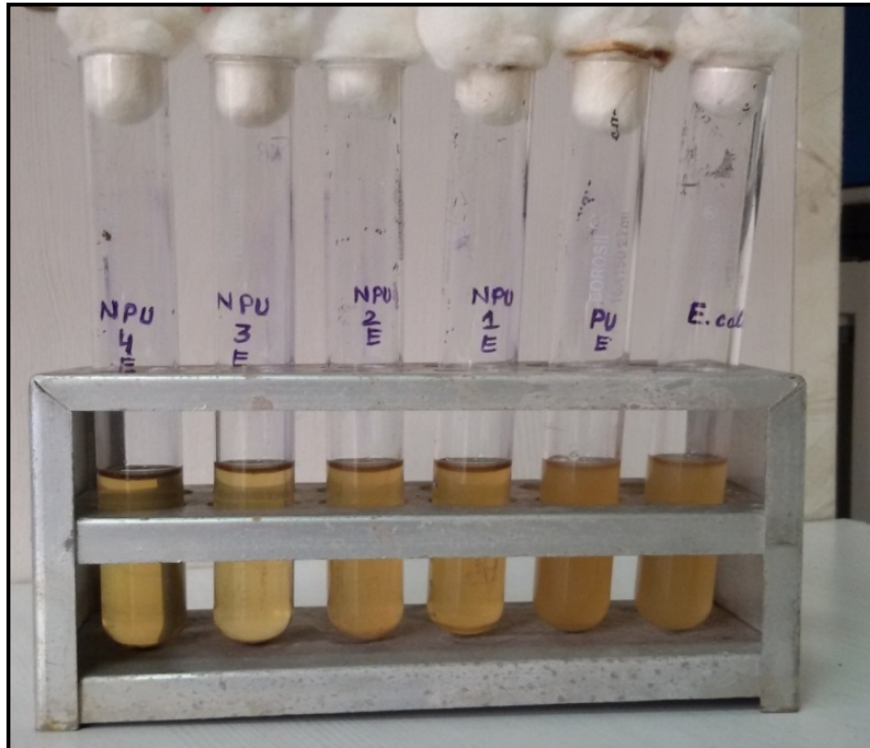


Figure 3.27 (ii): Antimicrobial activity of lignopolyol based polyurethane nanocomposite with varying filler concentration from 0-15% against *E.coli*

Further, it was also observed that with increase in % CNF loading in polyurethane, appreciable increase in activity towards *S. aureus* was observed than that of *E. coli*. The difference may be attributed to the difference in the bacterium cell structures and result of surrounding environmental factors.

Overall it was concluded that the lignopolyol based polyurethane nanocomposite films can inhibit the bacterial growth, thus can be optimally utilized in biomedical field.

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